

LBM Engineering, LLC

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CIVIL ENGINEERING - LAND DEVELOPMENT - SITE PLANS - STORMWATER MANAGEMENT

**Stormwater Management Report
For Land Use Commissions Submittals
Avery Brook Homes Subdivision,
Stoddards Wharf Road, Ledyard, Connecticut**

May 20, 2024

EXISTING CONDITIONS: Reference is made to the following Plan Set: "Plan Showing Resubdivision Property of Avery Brook Homes LLC 96, 98 and 100 Stoddards Wharf Road, A.K.A. Connecticut Route 214 Ledyard, Connecticut" Scales as Shown , March 2024, By Dieter & Gardner, Gales Ferry, CT. The property is located on the north side of Stoddards Wharf Road approximately one quarter mile east of the intersection of Whalehead Road and Stoddards Wharf Road. The property is wooded. The property drains primarily to the east and north.

STORMWATER MANAGEMENT: The Rational Method was used to analyze stormwater runoff in accordance with the Town of Ledyard's Ordinance Regulating the Management of Stormwater Runoff. This proposal will not increase the peak rate of runoff from the property nor will it increase the potential for downstream flooding. A Pre-Development versus Post- Development analysis is provided on Page 4 of the attached calculations,


WATER QUALITY: The Connecticut D.E.E.P. 2004 Stormwater Quality Manual (SWQM) defines the Water Quality Volume (WQV) as the volume of runoff from a one-inch rainfall event. SWQM Paragraph 7.4.1 states: "In the northeastern U.S., the 90 percent rainfall event is equal to approximately one inch, which is consistent with the recommended WQV sizing criteria for Connecticut." Therefore, by treating the WQV, the proposal effectively meets the requirements of the SWQM.

The subsoil throughout the property consists of sand and gravel with no evidence of seasonally high ground water. The soil conditions are excellent for infiltrating storm water. Therefore, roof runoff from each of the proposed homes will have an infiltration area, sized to hold and infiltrate the WQV thereby providing groundwater recharge per the SWQM guidelines. Surface water runoff is measurably reduced by infiltrating clean roof runoff back into the groundwater.

Runoff from roadway pavement drains to low-point catch basins and then piped to underground retention/infiltration areas where it is held and infiltrated into the subsoil. Proposed driveways will be gravel and stone to provide additional infiltration. Stormwater runoff leaves the property as sheet flow over wide areas. There are no point-discharges or channelized flows to cause erosion.

CONCLUSION: The proposed development meets the requirements of the Connecticut D.E.E.P. 2004 Stormwater Quality Manual and will not have adverse effects on down-gradient properties. This proposal will not increase the peak rate of runoff from the property nor will it increase the potential for downstream flooding and is in keeping with the policies and goals of the Ledyard Planning and Zoning Commission.

Submitted by:
LBM Engineering, LLC


John R. Martucci, P.E.



PREPARED BY JRM	DATE PREPARED 3/2024	LBM Engineering, LLC 11 HALLY LANE COLCHESTER, CONNECTICUT 06415 TEL: (860)-416-9809 EMAIL: JOHN@LBMENGINEERING.COM	JOB NUMBER	PAGE NUMBER 1
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AVERY BROOK DRAINAGE

AREA A SEE RATIONAL METHOD NOTE ON PAGE 3 AREA 1

PAVEMENT $I = 5.5''/HR$
 16,395 SF $290' \times 11' = 3190 SF$ 0.07 AC TO CB2
 0.38 AC.

$0.38 AC - 0.07 = 0.31 AC$ OVERLAND

$Q_{25} = 0.31 \times 0.21 \times 5.5 = 0.4 CFS$

POST DEVELOPMENT: PAVEMENT WILL GO TO CB1 AND THEN TO RETENTION AREA 1. REMAINDER WILL SHEET FLOW OFF

AREA B

PAVEMENT
 30,900 SF = 0.71 AC $290' \times 11' = 3190 SF = 0.07 AC$
 $0.71 AC - 0.07 AC = 0.64 AC$ TO RETENTION AREA 1

$0.71 AC - 0.07 AC = 0.64 AC$ OVERLAND

2 HOUSES - 0.04 AC 0.60 AC O'LAND

PAVT $0.07 \times 0.95 = 0.067$

O'LAND $0.60 \times 0.21 = 0.126$

0.193 $0.193 / 0.067 = 0.29$ WEIGHTED C

AREA C

$Q_{25} = 0.67 \times 0.29 \times 5.5 = 1.1 CFS$

83,740 SF = 1.92 AC - (6 HOUSES) 0.12 AC

1.8 ACRES O'LAND

$Q_{25} = 1.8 \times 0.21 \times 5.5 = 2.1 CFS$

ROOF RUNOFF

ROOF RUNOFF FROM EACH LOT WILL BE INFILTRATED

$36' \times 24' = 864 FT^2$ $864 / 12 = 72 FT^3 / INCH$
 (0.02 AC.)

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AREA D

$$49,342 \text{ SF} = 1.13 \text{ AC} - (10,600 \text{ SF PAVEMENT} = 0.24 \text{ AC})$$

$$1.13 \text{ AC} - (0.24 + (4 \text{ HOUSES}) + 0.08 \text{ AC}) = 0.81 \text{ AC O'LAND}$$

$$0.24 \times 0.95 = 0.228$$

$$0.81 \times 0.21 = 0.170$$

$$0.398$$

WEIGHTED
"C"

$$0.398 / 1.05 = 0.38$$

$$0.38 \times 1.05 \times 5.5 = 2.2 \text{ CFS}$$

AREA E

$$17,680 \text{ SF} = 0.41 \text{ AC} - (1 \text{ HOUSE}) 0.02 \text{ AC} = 0.39 \text{ AC O'LAND}$$

$$0.39 \times 0.21 \times 5.5 = 0.5 \text{ CFS}$$

AREA F

$$21,620 \text{ SF} = 0.50 \text{ AC} - (1 \text{ HOUSE}) 0.02 \text{ AC} = 0.48 \text{ AC O'LAND}$$

$$0.48 \times 0.21 \times 5.5 = 0.6 \text{ CFS}$$

AREA G

$$54,165 \text{ SF} = 1.24 \text{ AC} - (4 \text{ HOUSES}) 0.08 \text{ AC} = 1.16 \text{ AC O'LAND}$$

$$Q_{25} \text{ } 1.16 \times 0.21 \times 5.5 = 1.3 \text{ CFS}$$

TO CB1

10 MIN T_c 25 YR INTENSITY = $5.5 \frac{I}{HR}$

O'LAND RUNOFF C FOR TYPE A SOIL 0.21 (CONSERVATIVE)
FOR PAVEMENT 0.95

	AREA B	$A \times C$	
PAVT	$0.07 \times 0.95 =$	0.067	$(0.067 + 0.126) / 0.67 AC$ WEIGHTED C = 0.288
O'LAND	$0.60 \times 0.21 =$	0.126	

$Q_{TO CB1} = 0.67 \times 0.288 \times 5.5 = 1.06 CFS$

TO CB2

10 MIN T_c 25 YR $I = 5.5 \frac{I}{HR}$

$A = 290' \times 11' = 3190 SF = 0.07 AC$

$Q = C \times I \times A$ $C = 0.95$ $A = 0.07 AC$ $A \times C = 0.07 \times 0.95 = 0.066$

$Q = 0.066 \times 5.5 \frac{I}{HR} = 0.4 CFS$

RATIONAL METHOD NOTE: RATIONAL METHOD WAS USED TO COMPUTE PEAK RATES OF RUNOFF. DRAINAGE AREAS ARE SMALL (< 2 ACRES)

$Q_{25YR} = C I A$ $C_{PAVEMENT} = 0.95$ $C_{OVERLAND} = 0.21$
 $T_c = 10 MIN.$ $I = 5.5 \frac{I}{HR}$

PREPARED BY J. MARTUCCI	DATE PREPARED 5/2024	LBM Engineering, LLC 11 HALLY LANE COLCHESTER, CONNECTICUT 06415 TEL: (860)-416-9809 EMAIL: JOHN@LBMENGINEERING.COM	JOB NUMBER	PAGE NUMBER 4
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PRE VS. POST PEAK RATE OF RUNOFF COMPARISON

100 YR RAINFALL / C OVERLAND = 0.21 / 10 MIN T_c / I = 6.5" / HR

AREA A PRE 0.38 AC x 0.21 x 6.5 = 0.52 CFS
 POST FLOWS TO INFILTRATION AREA 1

AREA B PRE 0.71 AC x 0.21 x 6.5 = 0.97 CFS
 POST FLOWS TO INFLTN AREA 1
 INFILTRATION AREA 1 POST INFLOW = 2.03 CFS OUTFLOW 0.25 CFS

AREA C PRE 1.92 AC x 0.21 x 6.5 = 2.62 CFS
 POST (REMOVE HOUSES) 1.80 AC x 0.21 x 6.5 = 2.46 CFS

AREA D PRE 1.13 AC x 0.21 x 6.5 = 1.54 CFS
 POST FLOWS TO INFLTN AREA 2: INFLOW 2.46 CFS FLOW
 OUTFLOW 1.19 CFS

AREA E PRE 0.41 AC x 0.21 x 6.5 = 0.56 CFS
 POST 0.39 AC x 0.21 x 6.5 = 0.53 CFS

AREA F PRE 0.50 AC x 0.21 x 6.5 = 0.68 CFS
 POST 0.48 AC x 0.21 x 6.5 = 0.65 CFS

AREA G PRE 1.24 AC x 0.21 x 6.5 = 1.69 CFS
 POST 1.16 AC x 0.21 x 6.5 = 1.58 CFS

PEAK OFF PROPERTY A + B + C + D + E + F + G
 PRE 0.52 + 0.97 + 2.62 + 1.54 + 0.56 + 0.68 + 1.69 = 8.58 CFS
 INF AREA 1 OUT
 POST 0.25 + 2.46 + 1.19 + 0.53 + 0.65 + 1.58 = 6.66 CFS

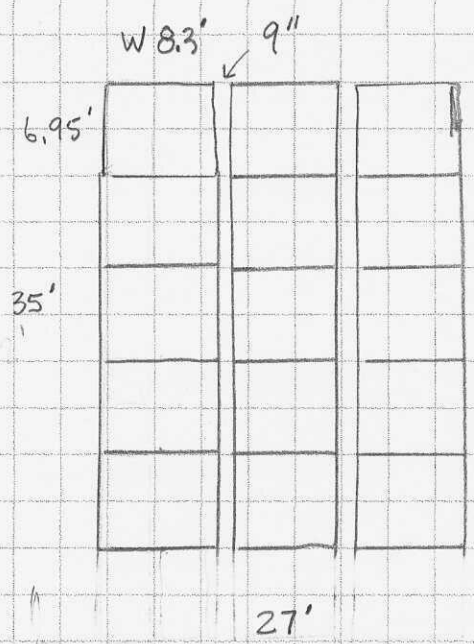
CONCLUSION: THE PROPOSAL WILL NOT INCREASE PEAK RATE OF RUNOFF FROM THE PROPERTY.

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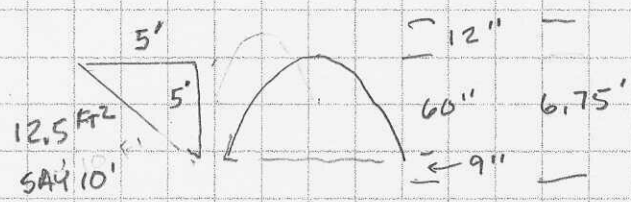
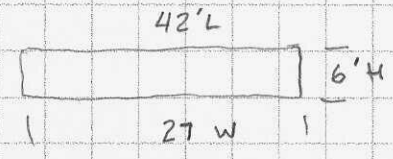
STORMTECH UNDERGROUND RETENTION AREAS



INSTALLED STORAGE
 267 FT³/CHAMBER
 267 x 15 = 4005

TOTAL 4005 + 245 = 4250 FT³ STORAGE

15 STORMTECH MC 7200



TOTAL VOL. 35 x 27 x 6 = 5670
 4250 / 5670 = 75% VOIDS

267 FT³ EACH INSTALLED CHAMBER

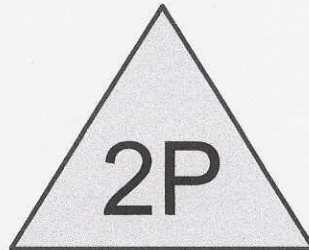
10' x 35' EACH SIDE

10' x 35' x 2 = 700 FT³ x 35% VOIDS = 245 FT³

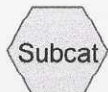
4250 / 6 = 708.3' PER FT OF DEPTH



AREA B



INFILTRATION 1



Routing Diagram for BASIN 1
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BASIN 1

CT-Ledyard 100-yr Duration=15 min, Inten=6.12 in/hr

Prepared by LBM Engineering LLC

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Summary for Subcatchment 1AB: AREA B

Runoff = 2.03 cfs @ 0.17 hrs, Volume= 2,737 cf, Depth= 0.71"
 Routed to Pond 2P : INFILTRATION 1

Runoff by Rational method, Rise/Fall=1.0/2.5 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
 CT-Ledyard 100-yr Duration=15 min, Inten=6.12 in/hr

Area (ac)	C	Description	Land Use
0.310	0.21	overland Area A	
0.600	0.21	overland Area B	
0.150	0.95	Pavement	
1.060	0.31	Weighted Average	
0.910		85.85% Pervious Area	
0.150		14.15% Impervious Area	

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, TO BASIN

Summary for Pond 2P: INFILTRATION 1

Inflow Area = 46,174 sf, 14.15% Impervious, Inflow Depth = 0.71" for 100-yr event
 Inflow = 2.03 cfs @ 0.17 hrs, Volume= 2,737 cf
 Outflow = 0.25 cfs @ 0.62 hrs, Volume= 81 cf, Atten= 88%, Lag= 26.8 min
 Primary = 0.25 cfs @ 0.62 hrs, Volume= 81 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
 Peak Elev= 143.06' @ 0.62 hrs Storage= 2,689 cf

Plug-Flow detention time= 36.6 min calculated for 80 cf (3% of inflow)
 Center-of-Mass det. time= 22.1 min (39.3 - 17.2)

Volume	Invert	Avail.Storage	Storage Description
#1	138.00'	3,188 cf	Custom Stage Data Listed below 4,250 cf Overall x 75.0% Voids

Elevation (feet)	Cum.Store (cubic-feet)
138.00	0
139.00	708
140.00	1,417
141.00	2,125
142.00	2,833
143.00	3,542
144.00	4,250

Device	Routing	Invert	Outlet Devices
#1	Primary	143.00'	6.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00

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BASIN 1

CT-Ledyard 100-yr Duration=15 min, Inten=6.12 in/hr

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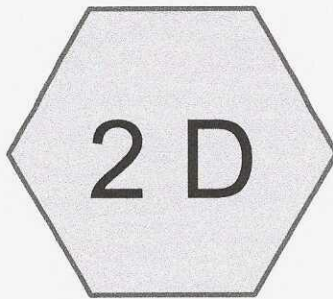
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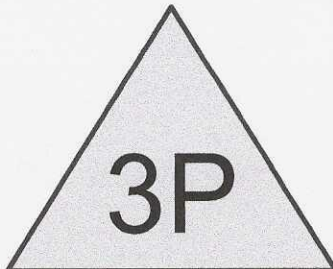
Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
3.30 3.31 3.32

Primary OutFlow Max=0.24 cfs @ 0.62 hrs HW=143.06' (Free Discharge)

↳ **1=Broad-Crested Rectangular Weir** (Weir Controls 0.24 cfs @ 0.67 fps)



2 AREA D



INFILTRATION 2



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BASIN 2

CT-Ledyard 100-yr Duration=15 min, Inten=6.12 in/hr

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Summary for Subcatchment 2 D: 2 AREA D

Runoff = 2.46 cfs @ 0.17 hrs, Volume= 3,324 cf, Depth= 0.87"
 Routed to Pond 3P : INFILTRATION 2

Runoff by Rational method, Rise/Fall=1.0/2.5 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
 CT-Ledyard 100-yr Duration=15 min, Inten=6.12 in/hr

Area (ac)	C	Description	Land Use
0.810	0.21	Overland Area D	
0.240	0.95	Pavement Area E	
1.050	0.38	Weighted Average	
0.810		77.14% Pervious Area	
0.240		22.86% Impervious Area	

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Direct Input - Small Areas

Summary for Pond 3P: INFILTRATION 2

Inflow Area = 45,738 sf, 22.86% Impervious, Inflow Depth = 0.87" for 100-yr event
 Inflow = 2.46 cfs @ 0.17 hrs, Volume= 3,324 cf
 Outflow = 1.19 cfs @ 0.47 hrs, Volume= 667 cf, Atten= 52%, Lag= 17.8 min
 Primary = 1.19 cfs @ 0.47 hrs, Volume= 667 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
 Peak Elev= 143.18' @ 0.47 hrs Storage= 2,750 cf

Plug-Flow detention time= 25.1 min calculated for 665 cf (20% of inflow)
 Center-of-Mass det. time= 14.4 min (31.6 - 17.2)

Volume	Invert	Avail.Storage	Storage Description
#1	138.00'	3,188 cf	Custom Stage Data Listed below 4,250 cf Overall x 75.0% Voids

Elevation (feet)	Cum.Store (cubic-feet)
138.00	0
139.00	708
140.00	1,417
141.00	2,125
142.00	2,833
143.00	3,542
144.00	4,250

Device	Routing	Invert	Outlet Devices
#1	Primary	143.00'	6.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31

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BASIN 2

CT-Ledyard 100-yr Duration=15 min, Inten=6.12 in/hr

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3.30 3.31 3.32

Primary OutFlow Max=1.19 cfs @ 0.47 hrs HW=143.18' (Free Discharge)

↑1=**Broad-Crested Rectangular Weir** (Weir Controls 1.19 cfs @ 1.13 fps)

The final element to be factored into the determination of runoff coefficients is the land slope. As the slope of the drainage basin increases, the selected C value should also increase. This is caused by the fact that as the slope of the drainage area increases, the velocity of overland and channel flow will increase allowing less opportunity for water to infiltrate the ground surface. Thus, more of the rainfall will become runoff from the drainage area.

In summary, it should be reiterated that in assigning a value to the runoff coefficient for use in the rational method, the engineer must rely heavily on experience and judgement.

Table 6-3 Recommended Coefficient Of Runoff For Pervious Surfaces By Selected Hydrologic Soil Groupings And Slope Ranges

<u>Slope</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>	
Flat (0 - 1%)	0.04-0.09	0.07-0.12	0.11-0.16	0.15-0.20	TYPE A SOIL AVERAGE SLOPE USED 0.21 TO BE CONSERVATIVE
Average (2 - 6%)	0.09-0.14 USE 0.21	0.12-0.17	0.16-0.21	0.20-0.25	
Steep (Over 6%)	0.13-0.18	0.18-0.24	0.23-0.31	0.28-0.38	

Source: Storm Drainage Design Manual, Erie and Niagara Counties Regional Planning Board.

Table 6-4 Recommended Coefficient Of Runoff Values For Various Selected Land Uses

<u>Description of Area</u>	<u>Runoff Coefficients</u>
Business: Downtown areas	0.70-0.95
Neighborhood areas	0.50-0.70
Residential: Single-family areas	0.30-0.50
Multi units, detached	0.40-0.60
Multi units, attached	0.60-0.75
Suburban	0.25-0.40
Residential (0.5 ha (1.2 ac) lots or more)	0.30-0.45
Apartment dwelling areas	0.50-0.70
Industrial: Light areas	0.50-0.80
Heavy areas	0.60-0.90
Parks, cemeteries	0.10-0.25
Playgrounds	0.20-0.40
Railroad yard areas	0.20-0.40
Unimproved areas	0.10-0.30

Appendix B - Rainfall**RAINFALL – DURATION – FREQUENCY
RELATIONSHIPS FOR CONNECTICUT**

DURATION	RETURN FREQUENCY (Years)					
	2	5	10	25	50	100
Min	RAINFALL IN MM (INCHES)					
5	9.1(0.36)	11.4(0.45)	13.0(0.51)	15.2(0.60)	17.2(0.67)	18.5(0.73)
15	18.3(0.72)	22.6(0.89)	25.9(1.02)	30.5(1.20)	34.0(1.34)	37.6(1.48)
60	33.0(1.3)	43.2(1.7)	50.8(2.00)	58.4(2.30)	65.3(2.57)	71.1(2.80)
Hrs						
2	40.6(1.60)	54.6(2.15)	63.5(2.50)	72.4(2.85)	82.6(3.25)	91.4(3.60)
3	44.5(1.75)	61.0(2.40)	69.9(2.75)	82.6(3.25)	90.2(3.55)	101.6(4.00)
6	59.7(2.35)	74.9(2.95)	87.6(3.45)	101.6(4.00)	115.6(4.55)	127.0(5.00)
12	69.9(2.75)	90.2(3.55)	101.6(4.00)	123.2(4.85)	135.9(5.35)	152.4(6.00)
24	82.6(3.25)	106.7(4.20)	125.7(4.95)	146.1(5.75)	161.3(6.35)	177.8(7.00)
24 HOUR RAINFALL BY COUNTY						
Fairfield	83.8(3.3)	109.2(4.3)	127.0(5.0)	144.8(5.7)	162.6(6.4)	182.9(7.2)
Hartford	81.3(3.2)	104.1(4.1)	119.4(4.7)	139.7(5.5)	157.5(6.2)	175.3(6.9)
Litchfield	81.3(3.2)	104.1(4.1)	119.4(4.7)	139.7(5.5)	157.5(6.2)	177.8(7.0)
Middlesex	83.8(3.3)	106.7(4.2)	127.0(5.0)	142.2(5.6)	160.0(6.3)	180.3(7.1)
New Haven	83.8(3.3)	106.7(4.2)	127.0(5.0)	142.2(5.6)	160.0(6.3)	180.3(7.1)
New London	86.4(3.4)	109.2(4.3)	127.0(5.0)	144.8(5.7)	160.0(6.3)	180.3(7.1)
Tolland	81.3(3.2)	104.1(4.1)	121.9(4.8)	139.7(5.5)	157.5(6.2)	175.3(6.9)
Windham	81.3(3.2)	106.7(4.2)	121.9(4.8)	139.7(5.5)	157.5(6.2)	175.3(6.9)

Sources:

1. "Rainfall Frequency Atlas of the United States", Technical Paper No. 40, U.S. Department of Commerce, Weather Bureau.
2. NOAA Technical Memorandum "NWS Hydro-35", June 1977, U.S. Department of Commerce, National Weather Service.

Table B-1

DURATION (min)	DURATION (hr)	RAINFALL INTENSITY (in/hr)					
		2 Yr	5 Yr	10 Yr	25 Yr	50 Yr	100 Yr
5	0.08	4.6	5.5	6.0	6.7	7.3	7.8
6	0.10	4.4	5.2	5.8	6.5	7.0	7.5
7	0.12	4.2	5.0	5.5	6.2	6.8	7.2
8	0.13	4.0	4.8	5.3	6.0	6.5	7.0
9	0.15	3.8	4.6	5.1	5.7	6.2	6.7
10	0.17	3.6	4.3	4.8	5.5	6.0	6.5
11	0.18	3.4	4.2	4.7	5.3	5.8	6.3
12	0.20	3.3	4.0	4.5	5.1	5.6	6.1
13	0.22	3.1	3.8	4.3	5.0	5.4	5.9
14	0.23	3.0	3.7	4.2	4.8	5.3	5.7
15	0.25	2.8	3.5	4.0	4.6	5.1	5.5
16	0.27	2.8	3.5	3.9	4.5	5.0	5.4
17	0.28	2.7	3.4	3.8	4.4	4.9	5.4
18	0.30	2.7	3.3	3.8	4.4	4.8	5.3
19	0.32	2.6	3.2	3.7	4.3	4.7	5.2
20	0.33	2.5	3.2	3.6	4.2	4.6	5.1
21	0.35	2.5	3.1	3.5	4.1	4.5	5.0
22	0.37	2.4	3.0	3.4	4.0	4.4	4.9
23	0.38	2.3	2.9	3.4	3.9	4.3	4.8
24	0.40	2.3	2.9	3.3	3.8	4.2	4.7
25	0.42	2.2	2.8	3.2	3.7	4.2	4.6
26	0.43	2.2	2.7	3.1	3.7	4.1	4.5
27	0.45	2.1	2.7	3.0	3.6	4.0	4.4
28	0.47	2.0	2.6	3.0	3.5	3.9	4.3
29	0.48	2.0	2.5	2.9	3.4	3.8	4.2
30	0.50	1.9	2.4	2.8	3.3	3.7	4.1

Rainfall Intensity/Duration/Frequency Relationship for Connecticut (English Units)
Table B-2.1