11 Hally Lane, Colchester, CT 06415-2133 Phone 860-416-9809 Email John@LBMEngineering.com

CIVIL ENGINEERING - LAND DEVELOPMENT - SITE PLANS - STORMWATER MANAGEMENT

Exhibit # BD

Stormwater Management Report For Land Use Commissions Submittals Avery Brook Homes Subdivision, Stoddards Warf Road, Ledyard, Connecticut November 13, 2022 Rev. 02/20/2023

EXISTING CONDITIONS: Reference is made to the following Plan Set: "Plan Showing Resubdivision Property of Avery Brook Homes LLC 94, 96, 98 and 100 Stoddards Wharf Road, A.K.A. Connecticut Route 214 Ledyard, Connecticut" Scales as Shown July 2022, Revised February 13, 2023, By Dieter & Gardner, Gales Ferry, CT. The property is located on the north side of Stoddards Wharf Road approximately one quarter mile east of the intersection of Whalehead Road and Stoddards Wharf Road. The property is wooded. The property drains primarily to the east and north.

STORMWATER MANAGEMENT: Detention of peak flow rates is not proposed for this development. The Town of Ledyard's <u>Ordinance Regulating the Management of Stormwater Runoff</u>, Part I. Section 3. Paragraph C. states: "A zero percent increase in discharge characteristics is specifically not applicable in cases where the applicant can demonstrate that the runoff will discharge to the Thames River or Groton Reservoir system without increasing the potential of downstream flooding."

This proposal will not increase the potential for downstream flooding. The subdivision is located at the bottom of the Billings Avery Brook, 770-acre watershed. Runoff from the development will precede the peak flow in Billings Avery Brook, thereby having no effect on downstream flooding.

WATER QUALITY: The Connecticut D.E.E.P. 2004 Stormwater Quality Manual (SWQM) defines the Water Quality Volume (WQV) as the volume of runoff from a one-inch rainfall event. SWQM Paragraph 7.4.1 states: "In the northeastern U.S., the 90 percent rainfall event is equal to approximately one inch, which is consistent with the recommended WQV sizing criteria for Connecticut." Therefore, by treating the WQV, the proposal effectively meets the requirements of the SWQM.

The proposed drainage system (catch basins and culverts) captures runoff from 950 feet of paved road and 15 building lots and carries the flow to a water quality basin. The water quality basin is designed to hold the WQV for 12 hours to settle out the suspended solids. The water quality basin's outlet is an extended detention underdrain which further filters the outflow and meters the flow through the outlet structure. The basin has a riprap spillway for storms larger than one inch. The wide spillway and the underdrain outlet have flow velocities below two feet per second (2 FPS) which is sub-erosive on grass surfaces.

The subsoil throughout the property consists of sand and gravel with no evidence of seasonally high ground water. The soil conditions are excellent for infiltrating storm water. Therefore, roof runoff from each of the proposed homes will have an infiltration area, sized to hold and infiltrate the WQV thereby providing groundwater recharge per the SWQM guidelines. Surface water runoff is measurably reduced by infiltrating clean water back into the groundwater.

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CIVIL ENGINEERING - LAND DEVELOPMENT - SITE PLANS - STORMWATER MANAGEMENT Avery Brook Homes, $P.\ 2$

Vegetated filter strips are proposed along the portions of the road that are not curbed. Runoff from the pavement will sheet-flow into the adjacent lawn and landscaping thereby providing filtration and infiltration. Proposed gentile slopes and small drainage areas make the vegetated filter strips a suitable application.

AREA	TREATMENT
4.7 Acres	To Stormwater Quality Basin
0.15 Acres of Road to 0.15 Acres of Lawn	Sheet Flow to Vegetated Filter Strips
1.5 Acres Lawns and Driveways	Sheet Flow to Undisturbed Vegetation
2.7 Acres Undisturbed Vegetation	Treatment Not Required
9.2 Acres Total	

CONCLUSION: The proposed development meets the requirements of the Connecticut D.E.E.P. 2004 Stormwater Quality Manual and will not have adverse effects on down-gradient properties, nor will it increase the potential for downstream flooding and is in keeping with the policies and goals of the Ledyard Planning and Zoning Commission.

Submitted by:

LBM Engineering, LLC

John R. Martucci, P.E.

PREPARED BY	DATE PREPARED	LBM Engineering, LLC	JOB N
CHECKED BY	DATE CHECKED	11 HALLY LANE COLCHESTER, CONNECTICUT 06415 TEL: (860)-416-9809	CLIENT
	2/2023	EMAIL: JOHN@LBMENGINEERING.COM	

JOB NUMBER PAGE NUMBER

CLIENT NAME TOTAL PAGES

AUFRY BROOK HOMES

DRAINAGE AREA BREAKDOWN! TO DETERMINE WOULD

4. TACRES TOTAL TO ROADWAY STORMDRAINS

ROOF RUNOFF FROM HOUSES ARE PIPED TO STORMTECH CHAMPERS SIZED TO HOLD & INFILTRATE I" (ONE INCH) OF VOLUME

15 LOTS DRAIN TO STORM DRAIN, DEDUCT ROOF AREA; 15 x (26' x 36') = 14,040 SF = 0.32 ACRES

950' OF 22' WIDE ROAD = 20,900 SF = 6.48 AC

15 DRIVEWAYS - ASSUME PAVED TO BE CONSERVATIVE

4.7 AC TOTAL MINUS (0,32 AC, ROOFS + 0,48 AC ROAD + 0,24 AC DRIVE)
= 3.66 AC OVERLAND

0.48 AC ROAD + 0.24AC = 0,72 AC IMPERVIOUS

PRIVES

SEE "WATER QUALITY FLOW / WATER QUALITY VOLUME"

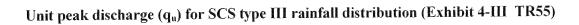
SPREAD SHEET

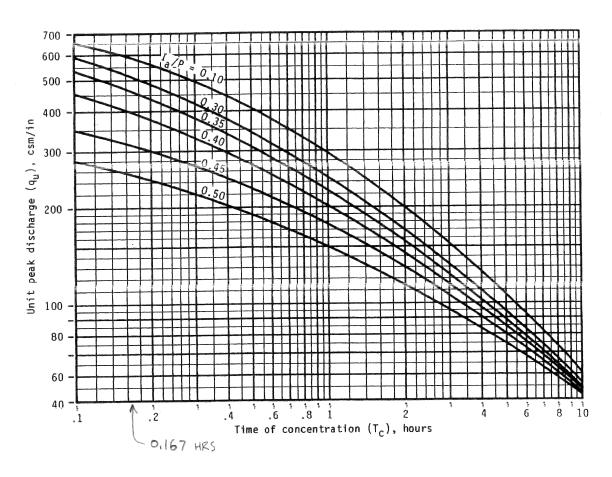
COMPUTATIO	NS FOR:						Project		
WATER QU	ΔΙ ΙΤΥ ΕΙ	OW / WAT	ER QUALI	TY VOLUM	IE		Made By:	JRM	
AVERY BROO	K HOMES S	UBDIVIDION			The second secon		Date:	8/3/2022	
LEDYARD									
							Date:	2/19/2023	
IN SYSTEM	TO BASIN							the second of the second	
ConnDOT D	rainage Ma	nual Ch 10	and Ch. 11	Appendix (3			and the second s	
GOIIIIDG I DI	Wooded	Grass		}					
Contributing	Area	Area	Paved	Total Area					
Basins	(acres)	(acres)	(acres)	(acres)					
TO BASIN	0	3 66	0.48	4.14					
			0.24	0.24					
							A CONTRACTOR OF THE PARTY OF TH		
Total	0	3.66	0.72	4.38					
Equation 10.	31: WQV =	(1")(R)(A)/12	=	0.072	acre-feet	or		cubic-feet	WQV
		<u> </u>			1		(3,900		-
I = % of Impe	ervious Cove	er=		16%			PROV	NOED)	
R = volumetr			009(1) =	0.1979					
A = site area			2 12 4 14 14 15 16 17 18 18 18 18 18	4.38	acres =	0.0068	miles ²		
and the second control of the second control of	I								
Q = runoff de	epth (in wate	ershed inches	s) = [WQV(a)]	acrefeet)]*[12	2(inches/foot	:)]/drainage a	rea (acres)		
		1	Q =	0.1979452					
	 				1				
CN = 1000 /	[10+ 5P + 1	$00.10(0^2 +$	1 25QP)0.51	=	86.0				
C14 = 10007	[10:01:1	10(0						1	1
P = design p	recinitation	(1" for water	quality storr	n) =	1	inch			
		ershed inches				1			
Q = ranon ac	spar (iii waa	3,0,,00			i	1			
t _c	10) min	The second secon						
t _c = 10 minu	4			0.167	hours			·	-
I _c = 10 minu	165 -								
E Table	4.4.1	0.326		la/P =	0.326				
From Table	4-1, la =	0.320		10/1 -	0.020				
Fara Falabiliti	. 4 111	500							
From Exhibit	4-111, q _u =	500					i		-
WOE /	(4)(0)	0.00	ofo		1			-	
WQF = (qu)	(A)(Q) =	0.68	CIS	1		· · · · · · · · · · · · · · · · · · ·	!	1	

Ia values for runoff curve numbers (Table 4-1 TR55)

Curve I _a	Curve I _a
number (in)	number (in)
403.000	700.857
412.878	710.817
422.762	720.778
432.651	730.740
442.545	740.703
452.444	750.667
462.348	760.632
472.255	770.597
482.167	780.564
492.082	790.532
502.000	800.500
511.922	810.469
521.846	820.439
531.774	830.410
541.704	840.381
551.636	850.353
561.571	860.326
571.509	870.299
581.448	880.273
591.390	890.247
601.333	900.222
611.279	910.198
621.226	920.174
631.175	930.151
641.125	940.128
651.077	950.105
661.030	960.083
670.985	970.062
680.941	980.041
690.899	

• Read the unit peak discharge (q_u) from Exhibit 4-III in Chapter 4 of TR-55 (reproduced below) for appropriate t_c





• Substituting the water quality volume (WQV), converted to watershed inches, for runoff depth (Q), compute the water quality flow (WQF) from the following equation:

$$WQF = (q_u)(A)(Q)$$

where: WQF = water quality flow (cfs) (English units only)

qu = unit peak discharge (cfs/mi²/inch)

A = drainage area (mi²)

Q = runoff depth (in watershed inches)

$$Q = \frac{[WQV(acrefeet]X[12(inches/foot]]}{DrainageArea(acres)}$$

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CHECKED BY	DATE CHECKED	11 HALLY LANE COLCHESTER, CONNECTICUT 06415 TEL: (860)-416-9809 EMAIL: JOHN@LBMENGINEERING.COM	CLIENT NAME	TOTAL PACES

DRAINAGE SYSTEM DESIGN

CB L STA 12+30 RT CB 2 STA 23+13 RT CB 3 STA 23+13 LT

CB1

STA 10+0 - 16+20 RIGHT SIDE OF ROAD

ROAD 620' × 11' = 6820 SF = 0.16 ACRES 'C'=0.19

CB 2

ROAD 630' × 11' = 6930 = 0.16 AC ROOF & DRIVEY 1500 SF × 2 LOTS = 3000 SF = 0,07 AC OVERLAND 16,200 SF = 0.37 AC TOTAL AREA 0,60 AC

WEIGHTED'C' [(0.23 × 0.9) + (0.37 × 0.3)] + 0.60 AC = 0.53

CB 3

ROAD 750' × 11' = 8250 SF = 0.19 AC

ROOF & DRIVES 1500 × 6 LOTS = 9,000 SF = 0.21 AC

OVERLAND 50,095 SF = 1.15 AC (1.55 +OTAL)

WEIGHTED'C'[(0.40 × 0.9) + (1.15 × 0.3)] + 1.55 = 0.45

11/12/22 Inlet Type <u>ا</u>رًا نِانِ AC Entering Catch Basin DATE: REV: DATE: 0.318 0.698 AC Bypassing (Inlet JRM SEE LOW POINT ANALYSIS SEE LOW POINT ANALYSIS SEE LOW POINT ANALYSIS Guller Flow Bypassing F Inlet (CIS) DESIGNED BY: CHECKED BY: Depth of C NOTES Cross Stope Of Shoulder ft/ft (Sx) G 0.043 0.043 GUTTER FLOW ANALYSIS - 25 YR STORM Grade of Gutter fuft (SL) Q to Inlet (cfs) 0.982 2.169 4.757 Total AC 0.144 0.698 0.144 0.698 AC 6.20 Rainfall Intensity (in/hr) 6.20 AVERY BROOK SUBDIVISION Time to Inlet 9 (min.) 5 5 0 Runoff Coeff. (C 0.45 0.53 6.0 PROPOSED ROAD RIGHT GUTTER PROPOSED ROAD LEFT GUTTER
CB 3 23+13, LT 1 550 Area in Acres (A) Ledyard Z/A LOW POINT ANALYSIS Inlet Station and Offset 12+30, RT 23+13, RT PROJECT: PROJECT NO.: ROUTE: LOCATION: CB 1 TOWN: Inlet ID

	AKEA	313	6.26	3.13	6.26
	PERIM	5.02	7 33	7.33	11.96
	GRATES	O	C DOUB	CL	CL DOUB
Notes	 Manning's n = 0.016 (asphalt) 	2.) Tc = 5 minutes minimum for areas with all pavement.	 Tc = 10 minutes minimum for small areas with pavement and grass. 	4) All low points operate as a wier. Depth (d) over grate is less than 0.4 feet	

<0.4' DEEP - OK <0.4' DEEP - OK <0.3' DEEP - OK

0.014 0.066 0.320

3.24 5.49 7.20

0.162 0.275 0.360

m m m

5.020 5.020 7.330

0.982 2.169 4.757

CB 1 CB 2 CB 3

d ORIFICE

WIDTH OF FLOW

C WEIR | d WEIR

PERIM.

Q TO INLET

INLET

STORM SEWER SYSTEM DESIGN

Client:
Project: AVERY BROOK SUBDIVISION
Proj. No.:
Return Period for Design: 25-YR

Prepared By: JRM

Date: 11/12/22 Revised: 12/12/22

Sheet No. 1 of 1

П	б	Т	Т	Т	Т	Т	Т	 Γ	T	٦	 -		 T	T	
	Mannin	<u>"</u> _		0.012	0.012	0.012									
	Headwater	(ft.)		0.50	0.50	08.0									
	Avg. Vel. Full Cap. Headwater Manning	(c.f.s.)		7.82	7.82	15.32									 -
Pipe Data	Avg. Vel.	(f.p.s.) (c.f.s.)		5.0	5.0	8.0									-
	Slope	(ft./ft.)		0.013	0.013	0.048		_							-
	Length	(ft.)		32	24	42									
	Size	(in.)		15	15	15		-							
ï	System	(c.f.s.)		4.33	6.30	7.19		-			gry and S				
Rainfall	Intensity,	System R (in./hr.) (c.f.s.)		6.2	6.2	6.2									
Sum of	A x C in			0.698	1.016	1.16									
A×C		System		0.698	0.318	0.144									
Accumul	Time	(min.)		10.0	10.1	10.2									
Time to Time in Accumul	Pipe	(min.)		0.11	0.08	60.0									
Time to	lalet Talet	(min.)		10	10	10									
	- tuent	- OL		CB 2											
	triange Section	From		CB 3	CB 2	CB 1									

Manning's "n" for, HDPE and RC pipe = 0.012

NOTE: ALL PIPES ARE BELOW FULL CAPACITY.

PREPARED BY	DATE PREPARED	LBM Engineering, LLC	JOB NUMBER	PAGE NUMBER
JRM	12/2022	11 HALLY LANE		
CHECKED BY	DATE CHECKED REV 2/2023	COLCHESTER, CONNECTICUT 06415 TEL: (860)—416—9809 EMAIL: JOHN@LBMENGINEERING.COM	CLIENT NAME	TOTAL PAGES

AVERY BROOK HOMES

CROSS CULVERT 11+12, LEFT TO 11+25, RIGHT - 25 YR STORM

82,580 SF TOTAL = 1.90 AC ROOF & DRIVES 1500 SF × 7 LOTS = 10,500 SF = 0.24 AC OVERLAND 1.90 - 0.24 = 1.66 AC

WEIGHTED C = [(0.24 × 0.9) + (1.66 × 0.3)] - 1.90 = 0.38

R=6.2"/hr 925= 1.9 AC × 6.2 × 0.38 = 4.5 CFS

USE 15"HOPE @ 1.1% SLOPE FULL CAPACITY 7.3 CFS

OMPUTATION	S FOR:					Project	
RIFICE SIZ	ING WORK	SHEET				Made By:	JRM
VERY BROOK		COLLET				Date:	11/13/2022
EDYARD, CT	HOFILS					Rev:	12/3/2022
EDTAKU, CI							
DIEICE SIZIN	IC EOR EX	TENDED DE	TENTION U	NDERDRAIN			
KIFICE SIZII	IO I ON EX	1211020 01		The second secon	2 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)		
	BASIN VOL	UME AT SP	ILLWAY = 4	300 CUBIC FT			
		DLUME (HA					
(ļ
ConnDOT Dra	inage Manı	ıal Equatioi	า 10.32				
							A CONTRACTOR OF THE PARTY OF
Qav = VOL./T		1000			100 mg		
OLUME (FT ³		4300				Market Control of the	
(SEC.)= 12 H	drs =	43,200	T 0 51	Holf Volomo			
Qav (CFS) =		0.0995	Target Q at	nali volottie			
100	States & Management Comment of the St			The second secon		Company of the Compan	
ConnDOT Dra	inage Man	ual Equatio	n 10.18		Q = Flow in CFS		
$Q = Kor D^2 Ho$	0.50	Kor =	3.78		Kor= Oriface Coefficien	t = 3.78	
2 - KOI D 110		1.01			D= Oriface		
HEAD AT FUL	1 = 25'	1		A SECTION OF THE PROPERTY OF T	H= Head in Feet		
D (inch)	D (FT.)	Н		Q (CFS)			
1.75	0.146	1.50		0.0985	1 min		
2.00	0.167	1.50		0.1286	USE 2" ORIFICE		
2.50	0.208	1.50	1	0.2009			
3.00	0.250	1.50		0.2893			
HEAD AT HAI	part described in the company of the			0 (050)		talent en	1
D (inch)	D (FT.)	Н	<u></u>	Q (CFS)	The state of the s		
1.75	0.146	0.75	1 T	0.0696	USE 2" ORIFICE		
2.00	0.167	0.75		0.0909 0.1421	USE Z UNIFICE		THE RESERVE AND A SECURE OF THE PARTY OF THE
2.50	0.208	0.75	1	0.1421		<u> </u>	
3.00	0.250	0.75		0.2040			
HEAD AT OF	e Santa de la casa de la La casa de la casa de	The second of th				, .,	
HEAD AT 0.5' D (inch)	D	Н	<u> </u>	Q (CFS)		Company of the second s	
1.75	0.146	0.50	1	0.0568			
2.00	0.143	0.50		0.0742	USE 2" ORIFICE		
2.50	0.208	0.50	-	0.1160			
3.00	0.250	0.50		0.1671			
	1			1			
007	LET RO	ATE OF	STORA	MWATER !	QUALITY BASIN	= 0.	CFS
yes, management and the second	1						
					The Company was to Commence the Commence of th		
		ļ					
	į.		1		i i		

CHANNEL DESIGN WORK SHEET

Client:

AVERY BROOK HOMES

Location: WATER QUAL BASIN

Town: LEDYARD

Return Period for Design: 1 INCH STORM

Prepared By: JRM

Date: 02/19/23

Checked By:

Revised:

Manning's equation - Q = (1.49/n) A R^{0.67} S^{0.5}

GRASS SWA	L	Е
------------------	---	---

Q_{CALC} (CFS)

V = Q/A (FPS)

GKASS SV	VALE			
YEAR	2	10	25	1-INCH
S (FT/FT)				0.01
d (FT)				0.08
W (FT)				2
A (SF)				0.1792
SS:1				3
R (A/WP)				0.0715
n				0.030

CHECKED IN BOX

THE CHANNEL WORKSHEET IS USED TO DETERMINE THE DEPTH OF FLOW "D" (d) AND THE VELOCITY OF FLOW "V".

0.152 0.8

2002 GUIDELINES P. 5-6-25 RIPRAP

0.034 MODIFIED 0.037 INTERMEDIATE 0.041 STANDARD

AFTER A I" STORM, * OUTLET OF STORMWATER QUALITY BASIN IS LESS THAN I' DEEP AND FLOWING AT LESS ! FT/SEC WHICH IS NOW EROSIVE IN A GRASS SWALE.



WQ BASIN



Reach



Link

Routing Diagram for BASIN WORKING

Prepared by LBM Engineering LLC, Printed 2/19/2023 HydroCAD® 10.20-2g s/n 09192 © 2022 HydroCAD Software Solutions LLC

CT-Ledyard 25-yr Duration=15 min, Inten=4.84 in/hr Printed 2/19/2023

Prepared by LBM Engineering LLC

HydroCAD® 10.20-2g s/n 09192 © 2022 HydroCAD Software Solutions LLC

Page 2

Summary for Subcatchment 1PR: TO BASIN

8.78 cfs @ 0.25 hrs, Volume= Routed to Pond 2P: WQ BASIN

13,804 cf. Depth= 0.87"

Runoff by Rational method, Rise/Fall=1.0/2.5 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs CT-Ledyard 25-yr Duration=15 min. Inten=4.84 in/hr

Area	(ac)	С	Des	cription		Land Use
3.	660	0.30	over	land		
0.	720	0.95	pave	ement and	driveways	
4.	380	0.41	Wei	ghted Ave	rage	
3.	3.660 83.56% Pervious Area					
0.	.720		16.4	4% Imper	vious Area	
Tc (min)	Leng (fe		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
15.0						Direct Entry, TO BASIN

Summary for Pond 2P: WQ BASIN

190,793 sf, 16.44% Impervious, Inflow Depth = 0.87" for 25-yr event Inflow Area =

8.78 cfs @ 0.25 hrs, Volume= 13,804 cf Inflow =

9,868 cf, Atten= 21%, Lag= 7.6 min 6.97 cfs @ 0.38 hrs, Volume= Outflow =

0.38 hrs, Volume= 9.868 cf Primary = 6.97 cfs @

Routing by Dyn-Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs Peak Elev= 146.42' @ 0.38 hrs Surf.Area= 3,704 sf Storage= 5,384 cf

Plug-Flow detention time= 14.9 min calculated for 9,868 cf (71% of inflow) Center-of-Mass det. time= 9.2 min (31.7 - 22.5)

Volume	Invert A	vail.Storage	Storage	Description		ann i de la companya di maga kandakan sa mulan ilah in kan manggaran mempilan pemenakan milan sa melili kan
#1	144.50'	5,683 cf	Custom	Stage Data (Pris	smatic) Listed bel	ow (Recalc)
Elevation (feet)	Surf.Are (sq-f		:.Store c-feet)	Cum.Store (cubic-feet)		
144.50 146.00 146.50	2,04 3,20 3,80	00	0 3,933 1,750	0 3,933 5,683		

Device	Routing	Invert	Outlet Devices
#1	Primary	146.00'	10.0' long x 8.0' breadth Broad-Crested Rectangular Weir
	,		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.43 2.54 2.70 2.69 2.68 2.68 2.66 2.64 2.64
			2.64 2.65 2.65 2.66 2.66 2.68 2.70 2.74

Primary OutFlow Max=6.97 cfs @ 0.38 hrs HW=146.42' (Free Discharge) 1=Broad-Crested Rectangular Weir (Weir Controls 6.97 cfs @ 1.66 fps) - MODIFIED RIPRAP

SPILLWAY LESS THAN ZFPS - NON EROSIVE ON GRASS, SUKFACE

