

# **Stormwater Management Report**

**Habitat For Humanity Residential Development** 

8, 9, and 11 Colby Drive, Ledyard CT

#### **Prepared For:**

## **Town of Ledyard**

741 Colonel Ledyard Highway Ledyard, CT 06339

## **Prepared By:**

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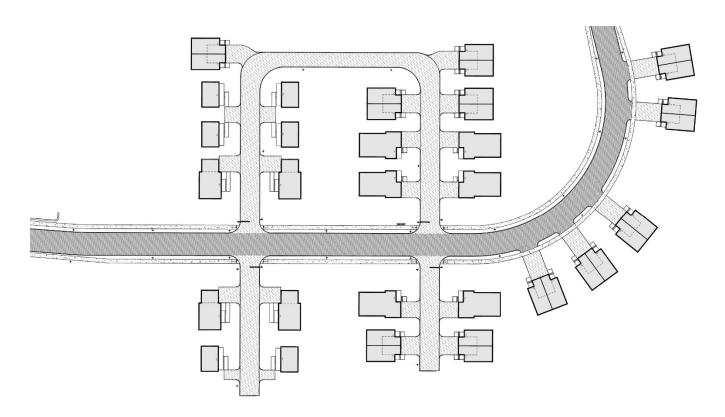
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## PROPOSED RESIDENTIAL DEVELOPMENT

(Schematic Layout)

8, 9, and 11 Colby Drive Ledyard, CT 06339



#### INTRODUCTION

#### 1.1 General Information

The subject parcels addressed 8, 9, and 11 Colby Drive, Ledyard, CT consist of approximately 15.71 acres and are located at the end of Colby drive, where it curves and extends down to Colonel Ledyard Highway. It is situated in the MFDD (Multi Family Development District) Zone and the subject parcels are denoted as and owned by:

- 8 Colby Drive Book 560 / Page 433 G Habitat for Humanity of Eastern CT Inc.
- 9 Colby Drive Book 560 / Page 436 G Habitat for Humanity of Eastern CT Inc.
- 11 Colby Drive Book 560 / Page 436 G Habitat for Humanity of Eastern CT Inc.
- Colby Drive Roadbed Book 560 / Page 442 Habitat for Humanity of Eastern CT Inc.

The project proposes the development of the existing parcels along with a full roadway construction to town standards. The proposed development will consist of twenty-seven (27) housing structures and the following site features:

- New Bituminous Pavement and Curbing
- New Concrete Walks
- Utilities and Storm Drainage system. (including detention)
- Revised Site Landscaping
- Single and Multi-Family Residential Buildings

The existing site is comprised of approximately 15.7 acres that is predominately wooded. This site has been the subject of multiple, various, applications over the past 40 – 50 years, all of which included the completion of a town road extending from the Colby Drive cul-de-sac through the site and connecting to Colonel Ledyard Highway. The natural low spot of the site is the northwestern portion, which is comprised of a large wetlands system. Based on discussions with town staff, it is our understanding that this wetlands system was utilized to provide stormwater management in the 1980s through the following construction:

- Construction of an earthen berm along the northern boundary line created a defined volume.
- A concrete outlet control structure, with a large RCP outlet pipe was placed to regulate flow out of the pond.
- The RCP pipe discharges to the property to the north (16 Highview Terrace). A stream has formed at this outlet pipe, and it runs south to north through the property. It appears a drainage easement was designed as part of a previous plan set, but the easement may have never been formalized and filed on the town land records.

This stormwater management system was designed to manage flow from the Colby Drive cul-de-sac development, as well as a previously approved development for the subject property (8, 9 and 11 Colby



Drive, and the Colby Drive Roadbed). The flows from the subject property were assumed to be generated by a 28' wide paved road extension (between the cul-de-sac and Colonel Ledyard Highway) and several commercial buildings. Therefore, the increased flows that truly need to be accounted for, for the proposed development, would only be the increased imperviousness from the previously approved commercial development and the proposed multi-family residential development.

However, the detention basin was never formally accepted by the Town. Therefore, in coordination with the Town staff, the proposed stormwater management has been designed with the following assumptions:

- The "existing" conditions consist of the current conditions (selectively cleared ROW and gravel drive) and NOT a 28' wide paved roadway with several commercial buildings. This resulted in the existing peak flows, as generated by the hydrologic model, being significantly lower than could perhaps take credit for. This forced us to design the proposed conditions to a much higher level of detention than would've otherwise been required.
- The Basin was surveyed and the topography was compared to the design plan from the 1990's. The comparison indicates the elevations and shape of the detention basin under current conditions is substantially in conformance with the original design in the 1980s. The Basin and structures were inspected and the facilities appear to be functioning as intended. We are providing several maintenance items in Section 2.3 of the report, which are to be expected after approximately 50 years, but the facility appears to be working as designed. Also, we have no knowledge of any complaints of flooding directly downstream of this basin.
- A new stormwater management system upgradient of the new paved road extension has been designed to manage and regulate all increased flows associated with the proposed development. This methodology has been designed to be very conservative, specifically to provide the Town with a level of comfort that the entirety of stormwater management will treat and regulate peak stormwater flow beyond that required by the applicable regulations. The proposed design assumes that the discharge point of our development is the existing detention basin on the northern portion of the property. peak flows are reducing from our site, to this basin, under proposed conditions for all the required design storms.

The proposed development includes an additional detention/infiltration basin and French drain to meet the 2024 CT DEEP Stormwater Quality Manual requirements for water quality and provide zero increase in runoff rate. Previously installed structures and pipes will be used if feasible after inspection and verification of suitability,





**Site Location Map** 

The project was designed utilizing the Town of Ledyard Zoning Regulations, the 2002 Connecticut Department of Transportation (ConnDOT) Drainage Manual, the latest Connecticut Guidelines for Soil Erosion and Sediment Control, and the latest Connecticut Department of Energy and Environmental Protection (CT DEEP) Water Quality Manual.



## 1.2 Project Summary

This project proposes to:

- Construct a new roadway for the town of Ledyard
- Construct multiple private driveways
- Construct multiple housing units
- Provide adequate site drainage and water quality.
- Provide ADA accessibility
- Construct utility connections to the buildings and site.

The project will disturb approximately 9.20 acres between the subject parcels and the ROW.

## 1.3 Existing Site Conditions

## 1.3.1 Topography

The project site slopes generally from south to north, with flow being directed to wetlands/existing detention basin northeast of the site. The proposed extension of Colby Drive is located within the previously approved right-of-way in approximately the same location. A portion of the drainage was previously constructed and will be inspected and reused to the extent possible. Elevations (NAVD 88) range from approximately 318 ft at the southern property border to 218 located at the northeaster property corner.

#### 1.3.2 Soils

NRCS soils mapping indicates 4 soil types located within the project limits; defined as:

- 47C Woodbridge Fine Sandy Loam Hydrologic Soil Group C
- 84B Paxton Montauk Fine Sandy Loam Hydrologic Soil Group C
- 85B Paxton Montauk Fine Sandy Loam Hydrologic Soil Group C
- 86B Paxton Montauk Fine Sandy Loam Hydrologic Soil Group C

Exploratory borings and test pits were completed onsite on October 24, 2024 and November 5, 2024 supervised by Down to Earth Consulting LLC. Groundwater was found to be 5-10.5 ft below the existing grade at ±257 and ±254 (NAVD 88). Infiltration testing was performed using the Falling Head Test. And revealed the pond location can infiltrate at a rate of 0.21in/hr, and a rate of 0.94in/hr at the location of the proposed French Drain.

The locations of Boring and Infiltration tests and results are included in Appendix G.



## 1.3.3 On-site and Adjacent Waterbody Information

There are wetlands adjacent to this project site. All flow from this site under existing conditions, both sheet flow and concentrated pipe flow, discharges to wetlands. This site is not located within an aquifer protection area, per Ledyard, CT Map (June 2024)

#### 1.3.4 Additional Site Considerations

- The existing stormwater management area has some organic overgrowth (phragmites, and down trees/root balls, etc.).
- The existing RCP discharge pipe into and out of the pond is not equipped with rip rap outlet control.
- The detention pond outlet control is comprised of a concrete block structure with a metal grate on the side (to prevent clogging of the low-flow orifice) and on top (to prevent clogging of the overflow spillway). Although the structure is structurally sound, the metal contains rust and the block mortar is slightly deteriorating in some locations.
- The site is currently undeveloped, except for the roughed in roadway, detention basin and catch basins which were installed for the previously approved roadway.
- A majority of existing soils have limiting exfiltration characteristics.
- The site is not located within a Natural Diversity Database Area, per Ledyard, CT Map, (June 2024)

#### **HYDROLOGY**

## 2.1 Methodology

The analysis to determine peak flows generated from the site was prepared using TR-55 procedures for calculating peak rates of runoff resulting from precipitation events and procedures for developing runoff hydrographs. HydroCAD software was utilized to perform hydrologic computations. Rainfall Frequency Estimates for precipitation frequency, based on National Oceanic and Atmospheric Administration (NOAA) data from Colby Drive, Ledyard, CT, were utilized to generate the flows. The following 24-hour, precipitation estimates were utilized:

2-Year	3.46 inches
10-Year	5.11 inches
25-Year	6.15 inches
50-Year	6.92 inches
100-Year	7.74 inches



Design Storm Type: NOAA, 24-hour Type D

Project Type: New Construction

## 2.2 Existing Conditions

### 2.2.1 Watershed Boundaries and Design Points.

Drainage from the existing site is contained within one (1) watershed for analysis.

• Watershed E1 (To Wetlands): This watershed consists of the entirety of the existing site. There is a previously graded, but unconstructed roadway designed directly through the middle of the site. The roadway was analyzed as constructed, along with the water which comes down the hill from outside the property onto the site. The majority of the existing site is a heavily wooded area, with some impervious cover. All flow from this watershed discharges through the existing detention pond to the wetlands or directly to the wetlands located northeast of the project site.

Existing Watershed Data (Existing Cover Characteristics, Existing Watershed Area Map, and Hydrologic Computations) have been included in Appendix A.

## 2.3 Proposed Conditions

## 2.3.1 Watershed Boundaries and Design Points

This project proposes to provide stormwater management in the form of a detention pond. Peak flow reduction is achieved using an outlet control structure to control stormwater discharge from the pond. The elevation of the bottom orifice and pond size have been calculated to meet the water quality requirement for the entire site. Drainage from the proposed site consists of two (2) subwatersheds for analysis.

- Watershed 1: This watershed has been further divided into subwatersheds for further analysis
  - Watershed P1-1 (Direct to Wetlands): This watershed consists of the area along the Eastern and northern borders on the downslope of the roadway, including a portion of the roadway, and a minor section of the slope from the pond. There is impervious cover from thirteen (13) Single and multi-family residential buildings, two (2) private drives and a portion of the proposed Colby Drive extension. There is proposed grass around all areas in this watershed which have been designed to be disturbed and regraded.
  - Watershed P1-2 (To Detention Pond): The majority of Colby Drive is within this watershed. Along with Colby Drive, there is a proposed private drive loop, fourteen (14)



proposed residential buildings and, pavement from offsite which sheet flows downhill from the west, to make up the proposed impervious cover of this watershed. The proposed detention pond and all disturbed areas around the proposed residential buildings make up the grass cover for this watershed. There is woodland offsite to the west and south which remains undisturbed and remains the same condition as existing.

Proposed Watershed Data (Proposed Cover Characteristics, Proposed Watershed Area Map, and Hydrologic Computations) have been included in Appendix B.

## 2.3.2 Existing Detention Basin Renovations

Based upon our site walk, following are the proposed renovations to the existing stormwater detention basin:

- Selectively remove the phragmite stand, as well as downed trees, stump and associated root balls in the area adjacent the pond inlet pipe.
- Place rip rap outlet control at the end of the existing RCP discharging into and out of the detention pond. The rip rap has been sized per ConnDOT criteria and the computations are shown in Appendix H.
- Remove the rust off the outlet control structure metal grates and remove the moss off the concrete block portion of the structure.
- Parge the interior portion of the concrete block structure to address the slight deterioration of existing mortar.

## 2.4 Compliance with Performance Criteria

## 2.4.1 Compliance with Local Criteria

This project has been designed per the Town of Ledyard's Stormwater Management Regulations.

## 2.4.2 Compliance with Connecticut Stormwater Quality Manual

## 2.4.2.1 Standard 1 – Runoff Volume Reduction

The method of analysis for this stormwater management system is providing site specific peak runoff volume reduction for the 2, 10, 25, 50, or 100-year Type NOAA, 24-hr Type D storm.

Low impact development practices have been implemented throughout this stormwater management design utilizing a series of treatment practices to remove temporarily suspended solids from the discharge location. Under existing conditions there are multiple catch basins and double catch basins,



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none of which receive significant flow as they have been set to the proposed elevation of the previously approved roadway and grading has only been performed to subgrade.

For the proposed detention pond, infiltration testing revealed an infiltration rate of 0.21in/hr. For the proposed French drain, infiltration testing revealed an infiltration rate of 0.94 in/hr. The French Drain has been modeled as a narrow but long infiltration basin to accommodate offsite flow.

Water quality volume calculations are provided in Appendix D.



## **Peak Flow Comparison**

Peak flows at the off-site analysis point are as follows:

#### **Proposed Watershed Hydrologic Characteristics** Colby Drive Ledyard, CT Project # 0725-500010.00

#### Comparison of Existing to Proposed Peak Flow Rate Watershed Storm Event (NOAA Type D) **Existing Flow (cfs)** Proposed Flow (cfs) 2-year 14.98 7.83 10-year 30.78 25.98 To Wetlands 25-year 41.66 41.15 49.91 45.72 50-year 100-year 58.82 50.73

Conclusion, total site peak flows will be reduced under proposed conditions for all design storms.

2.4.2.2 Standard 2 – Stormwater Runoff Quantity Control

See Peak Flow Comparison above.



#### **HYDRAULICS**

The intent of the hydraulic analysis is to ensure that proposed on-site drainage facilities are designed to accommodate and safely convey runoff produced up to and including the 25-year storm event.

### 3.1 Compliance with Performance Criteria

The site has been designed with a series of structural drainage facilities, including twenty-two (22) catch basins, four (4) double catch basins, eight (8) concrete area drains, one (1) dry well, one (1) French Drain, two (2) manholes, one (1) detention pond, four (4) flared end structures, one (1) outlet control structure and one (1) emergency overflow. This drainage system has been designed to remove stormwater from driving surfaces and divert it to the proposed detention pond, or directly to the wetlands.

## 3.1.1 Compliance with Local Criteria

The proposed storm sewer system has been designed in compliance with Town of Ledyard Drainage Regulations.

## 3.1.2 Compliance with State Criteria

The proposed storm sewer system has been designed in compliance with the State of Connecticut's drainage regulations per the 2002 ConnDOT Drainage Manual. (as amended)

Computations for the hydraulic analysis can be viewed in Appendix C.

#### WATER QUALITY

## 4.1 Methodology

The project has been designed to address both short-term and long-term stormwater quality. Short term (during construction) water quality has been provided in the form of erosion control measures and long-term (post construction) water quality has been provided through the use of primary and secondary treatment practices. Erosion control has been designed per the latest Connecticut Erosion Control Guidelines and long-term stormwater quality has been designed per the latest CT DEEP Stormwater Quality Manual.

## 4.2 Compliance with Performance Criteria

## 4.2.1 Compliance with Local Criteria

The proposed stormwater management system is designed to provide water quality volume for the entirety of the proposed development and treat the 1.3" storm as required by the 2024 CT DEEP Stormwater Quality Manual.



## 4.2.2 Compliance with Connecticut Stormwater Quality Manual

#### 4.2.2.1 Standard 1 – Pollutant Reduction

#### **Long Term Stormwater Quality**

The project was designed with guidance from the latest Connecticut Stormwater Quality Manual.

The site was designed to divert all surface stormwater to the proposed detention basin, where floatables, debris and other pollutants will be filtered out of the water prior to discharge to the onsite wetlands. The detention pond is designed to provide 100% of the required water quality volume.

Computations for Water Quality can be viewed in Appendix D.

#### SOIL EROSION AND SEDIMENT CONTROL

## 5.1 Methodology

The proposed soil erosion and sediment controls have been designed in accordance with local regulations, the Connecticut Guidelines for Soil Erosion and Sediment Control, and the requirements of the CTDEEP General Permit for the Discharge of Stormwater and Dewatering Wastewaters from Construction Activities, as applicable. The proposed design considers the specific site characteristics of the site and anticipated construction activities. See the plan set for location and design of proposed short term soil erosion and sediment control measures to be used throughout construction.

#### **Short Term Erosion Control**

The proposed erosion and sedimentation controls consider the specific characteristics of the site and the anticipated construction activities. They have been designed in accordance with the latest CT DEEP Guidelines for Soil Erosion and Sediment Control.

#### Construction Entrances

Construction entrances will be utilized to remove sediment from construction vehicle tires and prevent it from being tracked onto adjoining paved roadway areas.

#### **Erosion Control Barriers**

Prior to any construction activity, hay bales, silt fence, or combination hay bale/silt fence barriers will be placed at the downgradient limits of construction and adjacent to the wetlands. Throughout construction, additional barriers will be installed as necessary at the toe of slopes equal to or in excess of 15 feet. These barriers will be inspected once every seven calendar days



and within 24 hours after every rainfall generating a discharge and replaced as necessary. Collected silt will be removed when one-half the barrier height is reached.

#### **Temporary Seeding**

Temporary Seeding will be utilized on portions where the phasing and sequencing require an initial disturbance followed by an extended period of inactivity that is greater than 30 days but less than 1 year. Temporary seeding will be conducted within 7 days after the suspension of grading work in disturbed areas where the suspension of work is expected to be more than 30 days but less than 1 year.

#### Soil Stabilization- Mulches

Structural (non-living) soil stabilization will be utilized to protect the soil surface on a temporary basis without the intention of promoting plant growth. When grading of the disturbed area will be suspended for a period of 30 or more consecutive days, but less than 5 months, disturbed areas will be stabilized within 7 days of the suspension of grading through the use of mulch, nonbituminous tackifiers, erosion control netting, or other approved materials appropriate for use as a temporary soil protector. For surfaces that are not to be reworked within 5 months but will be reworked within 1 year, use temporary seeding, seeding-type mulch (hay, straw, or cellulose fiber) or when slopes are less than 3:1, wood chips, bark chips or shredded bark.

#### **Temporary Filter Inserts**

Temporary Filter Inserts will be placed in each existing catch basin and yard drains prior to the start of construction, and in each new catch basin or yard drain during construction. These devices will be removed upon final site stabilization. Filter inserts will be inspected once every seven (7) calendar days and within 24 hours after every rainfall generating a discharge. Replacement of the inserts will be as often as necessary to maintain function of the drainage structure and prevent excessive ponding due to clogged fabric. Ripped or otherwise damaged inserts will be replaced immediately.

#### Stockpile Management

The topsoil stockpiles which will be idle for at least 30 days will be stabilized with temporary seed and mulch no later than 7 days from the last use. Small stockpiles may be covered with impervious tarps or erosion control matting in lieu of seeding and mulching.

A geotextile silt fence or hay bale barrier will be installed around the stockpile area approximately 10 feet from the proposed toe of the slope.



#### 6 OPERATION AND MAINTENANCE

## **6.1 Inspection Frequency and Criteria**

Maintenance and operation will be provided as follows.

#### **During Construction**

- Dust Control: Moisten disturbed soil areas with water periodically, or use a non-asphaltic soil tacifier to minimize dust.
- **Temporary Soil Protection:** Inspect seeded areas weekly and within 24 hours after a storm generating a discharge.
- Catch Basin Filter Inserts: Inspect the fabric at least once a week and within 24 hours after the end of a storm generating a discharge. Check the fabric for structural soundness (i.e. tears), proper anchoring/alignment within the grate and ability to drain runoff (i.e. percent of clogging by sediment). Remove the sediment every week, or sooner if ponding is excessive. Each time the sediment is removed, replace the section of fabric removed with a new section. Do not remove the sediment and reuse the same section of fabric.
- Hay Bale/ Silt Fence Barrier: Inspect the barrier at least once a week and within 24 hours
  after the end of a storm generating a discharge. For dewatering operations, inspect
  frequently before, during and after pumping operations. Remove the sediment deposits
  when the depth reaches one half the barrier's height. Repair or replace a barrier within 24
  hours of observed failure. Maintain the barrier until the contributing disturbed area is
  stabilized.
- Construction Entrance/Exit Pad: Maintain the pad in a condition that will prevent tracking and washing of sediment onto paved surfaces. Place additional clean gravel on top of gravel that has become silted, or remove the silted gravel and replace the gravel to the depth removed with clean gravel, as conditions warrant. Remove immediately all sediment spilled, dropped, washed or tracked onto paved surfaces. Roads adjacent to the construction site shall be cleaned at the end of each day by hand sweeping or sweeper truck.
- **Existing Catch Basins and Sumps:** Inspect the filter baskets as specified above. After final removal of the filter baskets at the end of construction, clean the sump of all silt and debris.
- **New Catch Basins and Sumps:** As new catch basins are constructed, a sediment trap shall be installed in the unit and a sediment barrier installed around the grate. Inspect the



trap and barrier weekly and within 24 hours after a storm generating a discharge. After stabilization of the drainage area entering the catch basin, remove the trap and barrier and clean the basin sump of all silt and debris.

• **Temporary Stockpiles:** Inspect temporary stockpiles at the end of each workday to ensure that tarps are in place and secured. Temporary stockpiles that are expected to be inactive for more than 30 days should be temporarily seeded (see above).

#### **After Construction**

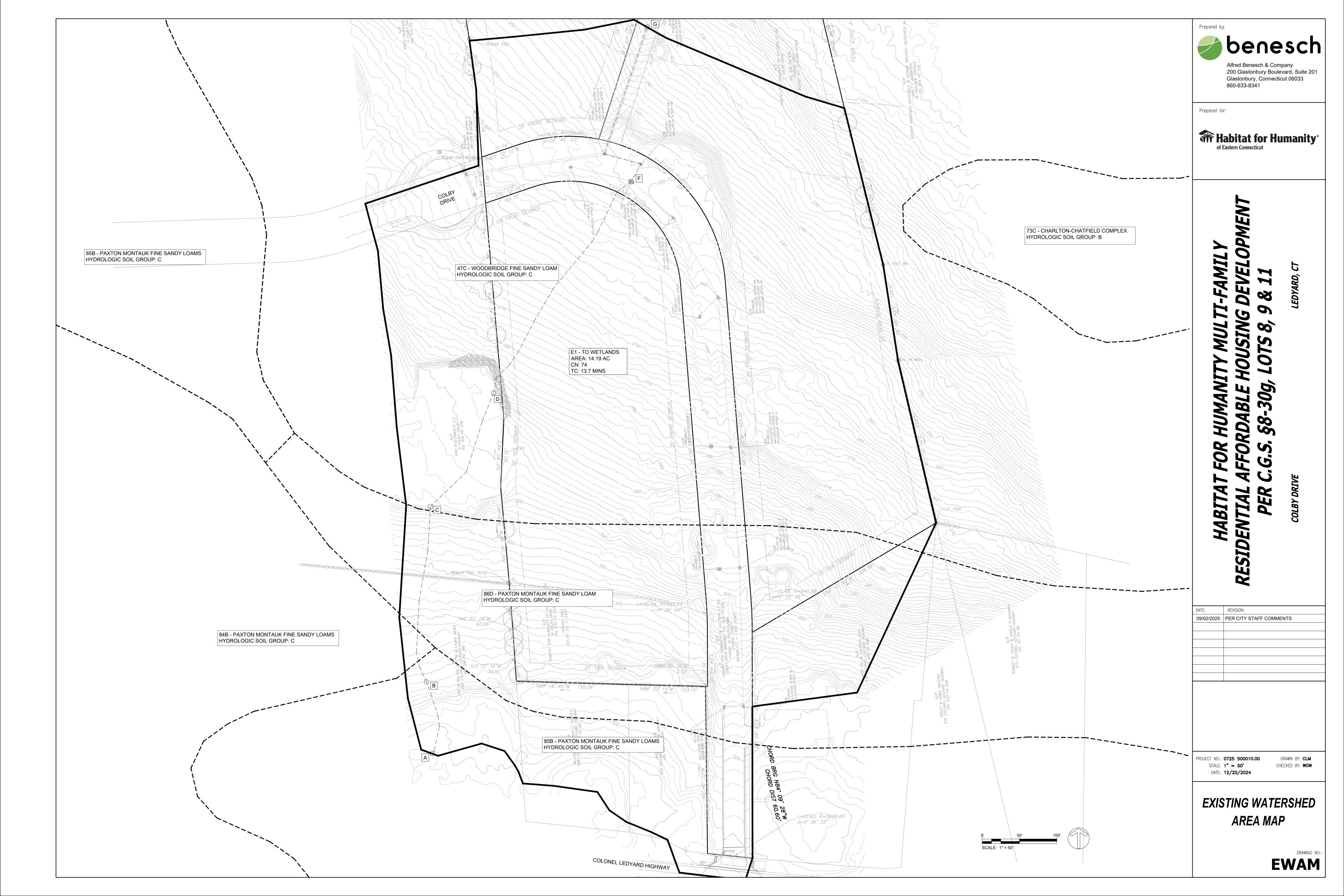
- Driveway Sweeping: At least twice a year, with the first occurring as soon as possible after snowmelt and the second not less than 90 days following the first.
- Catch Basins and Sumps: Maintenance includes removal of trash from the grate and the sump, as well as sediment from the sump. They shall be inspected semi-annually and cleaned when the sump is one half full of sediment. One of the inspections shall be after the snow and ice removal season is over, and prior to the spring rainfall events. If the sumps is filled more than half-filled with sediment at the semi-annual inspections, they shall be inspected quarterly.
- Landscaped Areas: Inspect semi-annually for erosion or dying vegetation. Repair and stabilize any bare or eroded areas and replace vegetation as soon as possible.
- **Detention Pond:** Inspect several times during the first few months to ensure that grass cover is established. Inspect the basin semi-annually and after major rain events for the first year, then annually after the first year. Trash should be removed as accumulated. Sediment building up should be removed when it's depth is greater than four (4) inches. Grass should be reseeded if the side slope or bottom exhibit erosion. Grass should be mowed once per month (depending on species) and should be cut to leave at least two (2) inches of height. Mowing should not occur when the ground is soft, to avoid rutting.
- **French Drain:** Inspect for sediment and debris build up on top of stone trench annually, if degradation of function is noticed and overflow flow is not contained within the drain, inspect pipe manually using a snake or camera equipment.



## **APPENDIX A**

**Existing Watershed Data** 

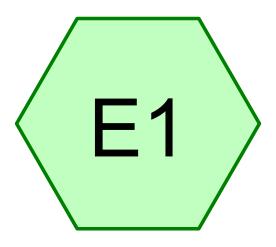




## Existing Watershed Cover Characteristics Colby Drive Ledyard, CT Project # 0725-500010.00

	Watershed Description		Woods	Gravel		CN	Tc (min)
Watershed		Total Area (AC)	С	С	Impervious		
watersneu			Good	W - ROW			
		70	89	98			
E1	To Wetlands	14.19	11.81	1.55	0.83	74	13.7

<sup>\* 1.38</sup> acres of gravel accounts for previously approved impervious surface discharge into existing detention basin



# To Wetlands









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## **Rainfall Events Listing**

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-year	NOAA10 24-hr	D	Default	24.00	1	3.46	2
2	10-year	NOAA 24-hr	D	Default	24.00	1	5.11	2
3	25-year	NOAA 24-hr	D	Default	24.00	1	6.15	2
4	50-year	NOAA 24-hr	D	Default	24.00	1	6.92	2
5	100-year	NOAA 24-hr	D	Default	24.00	1	7.74	2

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## **Area Listing (all nodes)**

Area	CN	Description
(acres)		(subcatchment-numbers)
1.550	89	Gravel roads, HSG C (E1)
0.830	98	Paved parking, HSG C (E1)
11.810	70	Woods, Good, HSG C (E1)
14.190	74	TOTAL AREA

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## Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
14.190	HSG C	E1
0.000	HSG D	
0.000	Other	
14.190		TOTAL AREA

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## **Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
 0.000	0.000	1.550	0.000	0.000	1.550	Gravel roads	E1
0.000	0.000	0.830	0.000	0.000	0.830	Paved parking	E1
0.000	0.000	11.810	0.000	0.000	11.810	Woods, Good	E1
0.000	0.000	14.190	0.000	0.000	14.190	TOTAL AREA	

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## Pipe Listing (all nodes)

Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Width	Diam/Height	Inside-Fill	Node
	Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)	Name
1	E1	0.00	0.00	257.0	0.0730	0.011	0.0	24.0	0.0	

NOAA10 24-hr D 2-year Rainfall=3.46"

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Time span=0.00-30.00 hrs, dt=0.05 hrs, 601 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: To Wetlands

Runoff Area=14.190 ac 5.85% Impervious Runoff Depth=1.21"

Flow Length=1,118' Tc=13.7 min CN=74 Runoff=14.98 cfs 1.434 af

Total Runoff Area = 14.190 ac Runoff Volume = 1.434 af Average Runoff Depth = 1.21" 94.15% Pervious = 13.360 ac 5.85% Impervious = 0.830 ac

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## **Summary for Subcatchment E1: To Wetlands**

Runoff = 14.98 cfs @ 12.22 hrs, Volume= 1.434 af, Depth= 1.21" Routed to nonexistent node TS

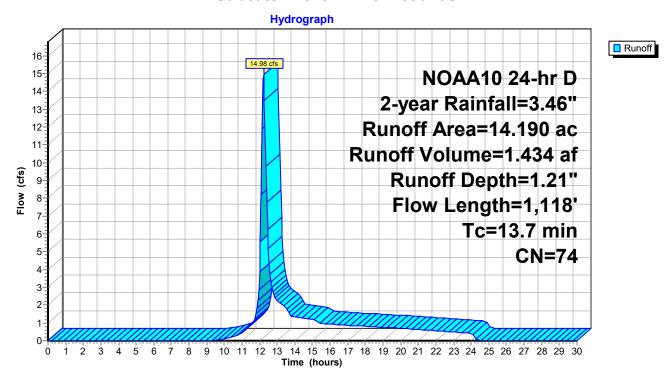
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA10 24-hr D 2-year Rainfall=3.46"

Area	(ac) C	N Desc	cription		
			ds, Good,		
			ed parking,		
			<u>rel roads, l</u>		
	14.190 74 Weighted Average				
	13.360 94.15% Pervious				
0.	0.830 5.85% Impervious Area			ous Area	
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	2 cccinpuon
10.8	100	0.1000	0.15	,	Sheet Flow, Woods
					Woods: Light underbrush n= 0.400 P2= 3.46"
8.0	239	0.0920	4.88		Shallow Concentrated Flow, Woods
					Unpaved Kv= 16.1 fps
8.0	179	0.0330	3.69		Shallow Concentrated Flow, Impervious
4.4	0.40	0.4400	E 0.4		Paved Kv= 20.3 fps
1.1	343	0.1100	5.34		Shallow Concentrated Flow, Woods Unpaved Kv= 16.1 fps
0.2	257	0.0730	22.99	72.24	Pipe Channel, pipe
0.2	201	0.0730	22.55	12.24	24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
					n= 0.011 Concrete pipe, straight & clean
13.7	1,118	Total			, ,g

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#### **Subcatchment E1: To Wetlands**



NOAA 24-hr D 10-year Rainfall=5.11"

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Time span=0.00-30.00 hrs, dt=0.05 hrs, 601 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: To Wetlands

Runoff Area=14.190 ac 5.85% Impervious Runoff Depth=2.45" Flow Length=1,118' Tc=13.7 min CN=74 Runoff=30.78 cfs 2.900 af

Total Runoff Area = 14.190 ac Runoff Volume = 2.900 af Average Runoff Depth = 2.45" 94.15% Pervious = 13.360 ac 5.85% Impervious = 0.830 ac

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### **Summary for Subcatchment E1: To Wetlands**

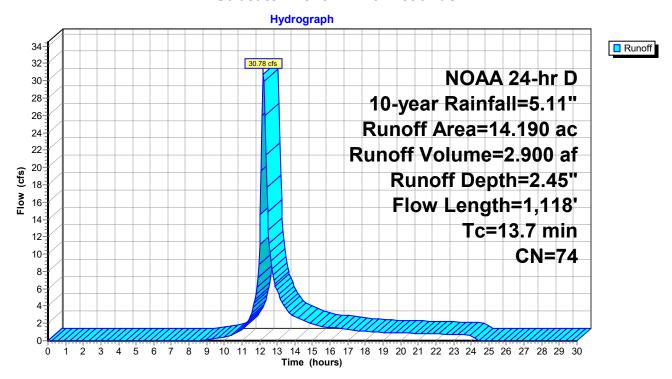
Runoff = 30.78 cfs @ 12.22 hrs, Volume= 2.900 af, Depth= 2.45" Routed to nonexistent node TS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 10-year Rainfall=5.11"

Area	(ac) C	N Desc	cription							
			ds, Good,							
	0.830 98 Paved parking, HSG C 1.550 89 Gravel roads, HSG C									
	190 7	'4 Weig	ghted Aver	age						
	360		5% Pervio							
U.	830	5.65	% Impervi	ous Area						
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
10.8	100	0.1000	0.15		Sheet Flow, Woods					
0.0	000	0.0000	4.00		Woods: Light underbrush n= 0.400 P2= 3.46"					
8.0	239	0.0920	4.88		Shallow Concentrated Flow, Woods Unpaved Kv= 16.1 fps					
0.8	179	0.0330	3.69		Shallow Concentrated Flow, Impervious					
					Paved Kv= 20.3 fps					
1.1	343	0.1100	5.34		Shallow Concentrated Flow, Woods					
0.2	257	0.0720	22.00	72.24	Unpaved Kv= 16.1 fps					
0.2	257	0.0730	22.99	72.24	Pipe Channel, pipe 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'					
					n= 0.011 Concrete pipe, straight & clean					
13.7	1,118	Total								

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#### **Subcatchment E1: To Wetlands**



NOAA 24-hr D 25-year Rainfall=6.15"

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Time span=0.00-30.00 hrs, dt=0.05 hrs, 601 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: To Wetlands

Runoff Area=14.190 ac 5.85% Impervious Runoff Depth=3.31" Flow Length=1,118' Tc=13.7 min CN=74 Runoff=41.66 cfs 3.916 af

Total Runoff Area = 14.190 ac Runoff Volume = 3.916 af Average Runoff Depth = 3.31" 94.15% Pervious = 13.360 ac 5.85% Impervious = 0.830 ac

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### **Summary for Subcatchment E1: To Wetlands**

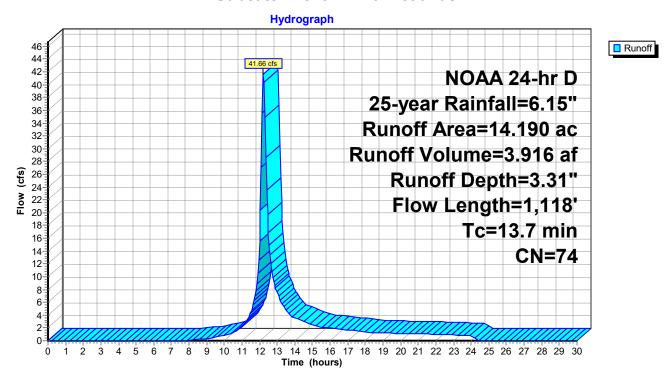
Runoff = 41.66 cfs @ 12.22 hrs, Volume= 3.916 af, Depth= 3.31" Routed to nonexistent node TS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 25-year Rainfall=6.15"

Area	(ac) C	N Desc	cription						
			ds, Good,						
	0.830 98 Paved parking, HSG C 1.550 89 Gravel roads, HSG C								
			ghted Aver						
	360 830	_	5% Pervio % Impervi						
0.	030	5.65	76 Impervi	ous Alea					
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
10.8	100	0.1000	0.15		Sheet Flow, Woods				
0.0	000	0.0000	4.00		Woods: Light underbrush n= 0.400 P2= 3.46"				
0.8	239	0.0920	4.88		Shallow Concentrated Flow, Woods Unpaved Kv= 16.1 fps				
0.8	179	0.0330	3.69		Shallow Concentrated Flow, Impervious				
0.0	110	0.0000	0.00		Paved Kv= 20.3 fps				
1.1	343	0.1100	5.34		Shallow Concentrated Flow, Woods				
					Unpaved Kv= 16.1 fps				
0.2	257	0.0730	22.99	72.24	Pipe Channel, pipe				
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.011 Concrete pipe, straight & clean				
40.7	4 440	Tatal			11- 0.011 Concrete pipe, straight & clean				
13.7	1,118	Total							

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#### **Subcatchment E1: To Wetlands**



NOAA 24-hr D 50-year Rainfall=6.92"

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Time span=0.00-30.00 hrs, dt=0.05 hrs, 601 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: To Wetlands

Runoff Area=14.190 ac 5.85% Impervious Runoff Depth=3.97" Flow Length=1,118' Tc=13.7 min CN=74 Runoff=49.91 cfs 4.697 af

Total Runoff Area = 14.190 ac Runoff Volume = 4.697 af Average Runoff Depth = 3.97" 94.15% Pervious = 13.360 ac 5.85% Impervious = 0.830 ac

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### **Summary for Subcatchment E1: To Wetlands**

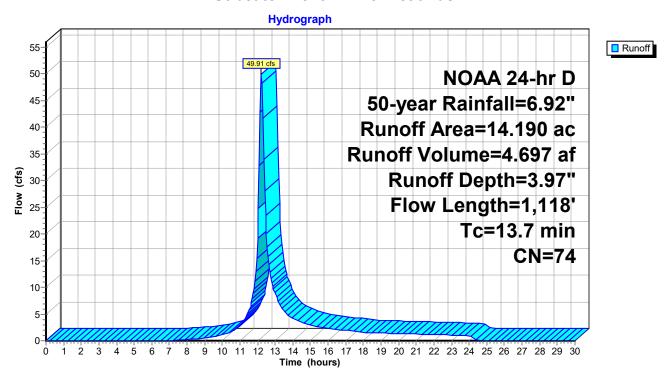
Runoff = 49.91 cfs @ 12.22 hrs, Volume= 4.697 af, Depth= 3.97" Routed to nonexistent node TS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 50-year Rainfall=6.92"

Area	(ac) C	N Desc	cription							
			ds, Good,							
	0.830 98 Paved parking, HSG C 1.550 89 Gravel roads, HSG C									
	190 7	'4 Weig	ghted Aver	age						
	360		5% Pervio							
U.	830	5.65	% Impervi	ous Area						
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
10.8	100	0.1000	0.15		Sheet Flow, Woods					
0.0	000	0.0000	4.00		Woods: Light underbrush n= 0.400 P2= 3.46"					
8.0	239	0.0920	4.88		Shallow Concentrated Flow, Woods Unpaved Kv= 16.1 fps					
0.8	179	0.0330	3.69		Shallow Concentrated Flow, Impervious					
					Paved Kv= 20.3 fps					
1.1	343	0.1100	5.34		Shallow Concentrated Flow, Woods					
0.2	257	0.0720	22.00	72.24	Unpaved Kv= 16.1 fps					
0.2	257	0.0730	22.99	72.24	Pipe Channel, pipe 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'					
					n= 0.011 Concrete pipe, straight & clean					
13.7	1,118	Total								

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#### **Subcatchment E1: To Wetlands**



NOAA 24-hr D 100-year Rainfall=7.74"

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Time span=0.00-30.00 hrs, dt=0.05 hrs, 601 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: To Wetlands

Runoff Area=14.190 ac 5.85% Impervious Runoff Depth=4.69"

Flow Length=1,118' Tc=13.7 min CN=74 Runoff=58.82 cfs 5.550 af

Total Runoff Area = 14.190 ac Runoff Volume = 5.550 af Average Runoff Depth = 4.69" 94.15% Pervious = 13.360 ac 5.85% Impervious = 0.830 ac

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### **Summary for Subcatchment E1: To Wetlands**

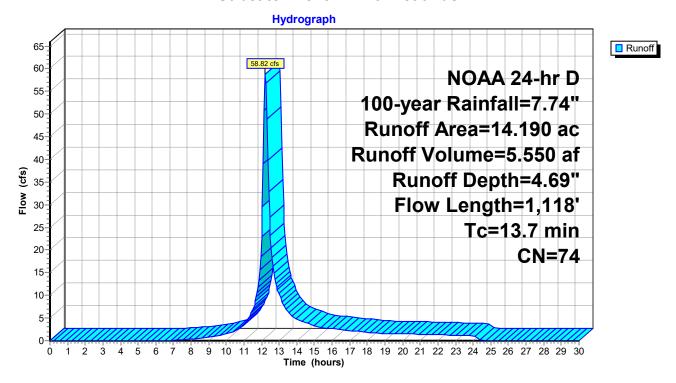
Runoff = 58.82 cfs @ 12.22 hrs, Volume= 5.550 af, Depth= 4.69" Routed to nonexistent node TS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 100-year Rainfall=7.74"

	Area	(ac) C	N Desc	cription		
	11.	810 7	0 Woo	ds, Good,	HSG C	
	0.	830 9	8 Pave	ed parking	, HSG C	
_	1.	550 8	39 Grav	∕el roads, l	HSG C	
	14.	190 7	'4 Wei	ghted Avei	age	
	13.	360	94.1	5% Pervio	us Area	
	0.	830	5.85	% Impervi	ous Area	
	_					<b>—</b>
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	10.8	100	0.1000	0.15		Sheet Flow, Woods
						Woods: Light underbrush n= 0.400 P2= 3.46"
	8.0	239	0.0920	4.88		Shallow Concentrated Flow, Woods
						Unpaved Kv= 16.1 fps
	8.0	179	0.0330	3.69		Shallow Concentrated Flow, Impervious
						Paved Kv= 20.3 fps
	1.1	343	0.1100	5.34		Shallow Concentrated Flow, Woods
		0.55	0.0700	00.00	70.04	Unpaved Kv= 16.1 fps
	0.2	257	0.0730	22.99	72.24	Pipe Channel, pipe
						24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
_						n= 0.011 Concrete pipe, straight & clean
	13 7	1 118	Total			

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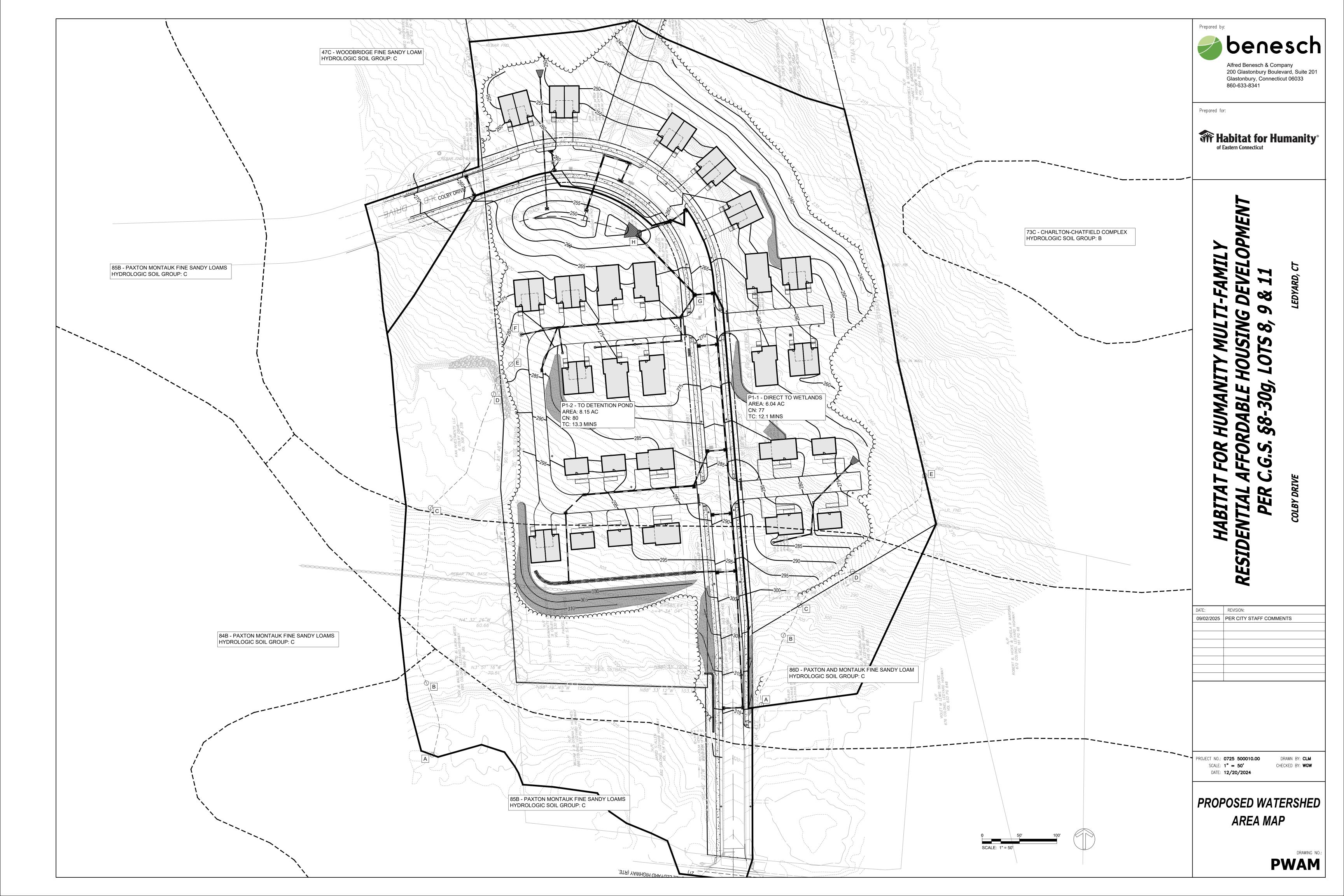
#### **Subcatchment E1: To Wetlands**



# **APPENDIX B**

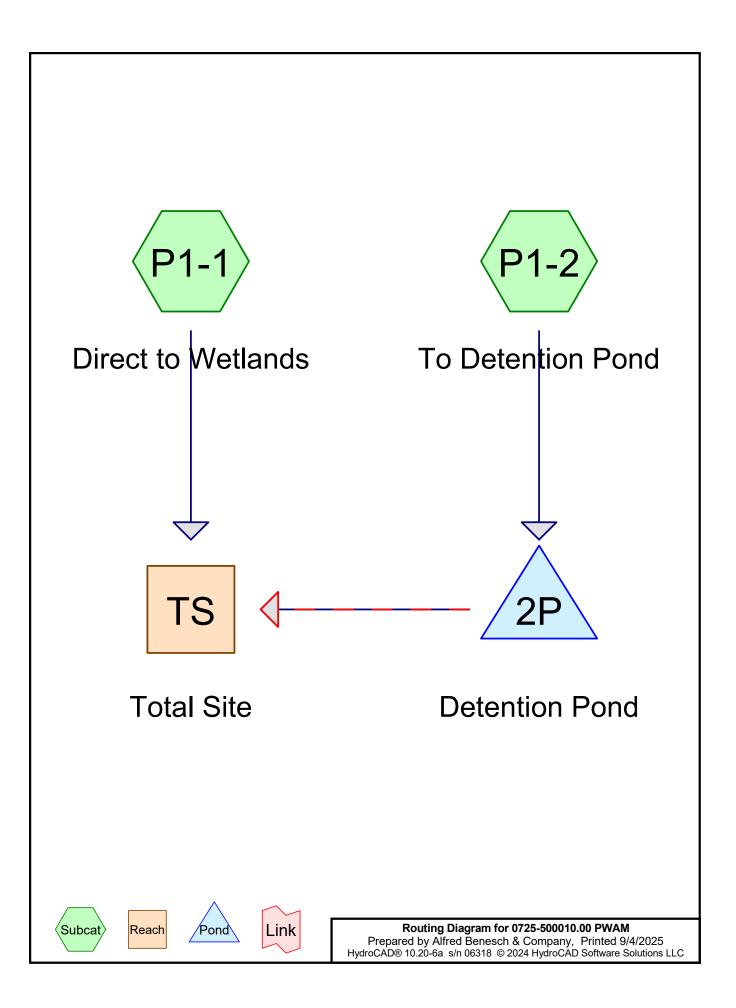
Proposed Watershed Data





#### Proposed Watershed Cover Characteristics Colby Drive Ledyard, CT Project # 0725-500010.00

			Woods	Grass	Grass		Tc (min)
Watershed	Description	Total Area	С	С	Impervious	CN	
Watershed	Description	(AC)	Good	good			
			70	74	98		
P1-1	Direct to Wetlands	6.04	2.68	2.15	1.22	77	12.1
P1-2	To Detention Pond	8.15	3.24	2.49	2.42	80	13.3
TS	Total Site	14.19	5.92	4.64	3.63	79	



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### **Rainfall Events Listing**

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-year	NOAA 24-hr	D	Default	24.00	1	3.46	2
2	10-year	NOAA 24-hr	D	Default	24.00	1	5.11	2
3	25-year	NOAA 24-hr	D	Default	24.00	1	6.15	2
4	50-year	NOAA 24-hr	D	Default	24.00	1	6.92	2
5	100-year	NOAA 24-hr	D	Default	24.00	1	7.74	2

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### **Area Listing (all nodes)**

Area	CN	Description
 (acres)		(subcatchment-numbers)
4.640	74	>75% Grass cover, Good, HSG C (P1-1, P1-2)
3.640	98	Paved parking, HSG C (P1-1, P1-2)
5.920	70	Woods, Good, HSG C (P1-1, P1-2)
14.200	78	TOTAL AREA

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### Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
14.200	HSG C	P1-1, P1-2
0.000	HSG D	
0.000	Other	
14.200		TOTAL AREA

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### **Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	4.640	0.000	0.000	4.640	>75% Grass cover, Good	P1-1,
							P1-2
0.000	0.000	3.640	0.000	0.000	3.640	Paved parking	P1-1,
							P1-2
0.000	0.000	5.920	0.000	0.000	5.920	Woods, Good	P1-1,
							P1-2
0.000	0.000	14.200	0.000	0.000	14.200	TOTAL AREA	

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### Pipe Listing (all nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Width (inches)	Diam/Height (inches)	Inside-Fill (inches)	Node Name
1	P1-2	0.00	0.00	250.0	0.0600	0.011	0.0	15.0	0.0	
2	P1-2	0.00	0.00	106.0	0.0058	0.011	0.0	24.0	0.0	
3	2P	254.60	252.50	74.0	0.0284	0.011	0.0	24.0	0.0	

NOAA 24-hr D 2-year Rainfall=3.46"

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Time span=0.00-30.00 hrs, dt=0.05 hrs, 601 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment P1-1: Direct to Wetlands**Runoff Area=6.050 ac 20.17% Impervious Runoff Depth=1.40"
Flow Length=409' Tc=12.1 min CN=77 Runoff=7.83 cfs 0.706 af

Subcatchment P1-2: To Detention Pond Runoff Area=8.150 ac 29.69% Impervious Runoff Depth=1.60" Flow Length=966' Tc=13.3 min CN=80 Runoff=11.70 cfs 1.090 af

Reach TS: Total Site Inflow=7.83 cfs 1.301 af
Outflow=7.83 cfs 1.301 af

**Pond 2P: Detention Pond**Peak Elev=256.91' Storage=22,022 cf Inflow=11.70 cfs 1.090 af Discarded=0.05 cfs 0.070 af Primary=2.51 cfs 0.595 af Secondary=0.00 cfs 0.000 af Outflow=2.56 cfs 0.664 af

Total Runoff Area = 14.200 ac Runoff Volume = 1.796 af Average Runoff Depth = 1.52" 74.37% Pervious = 10.560 ac 25.63% Impervious = 3.640 ac Prepared by Alfred Benesch & Company
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## Summary for Subcatchment P1-1: Direct to Wetlands

Runoff = 7.83 cfs @ 12.20 hrs, Volume= 0.706 af, Depth= 1.40"

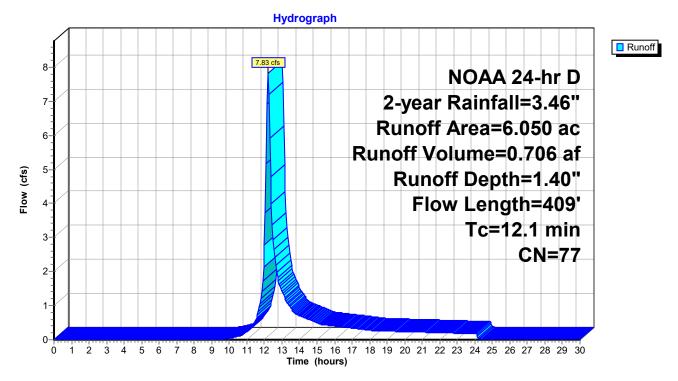
Routed to Reach TS: Total Site

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 2-year Rainfall=3.46"

Area	(ac) C	N Desc	cription		
2.	.680 7	'0 Woo	ds, Good,	HSG C	
2.	.150 7	'4 >75°	% Grass co	over, Good	, HSG C
1.	.220	8 Pave	ed parking	, HSG C	
6.	.050 7	7 Wei	ghted Aver	age	
4.	.830	•	3% Pervio	•	
1.	.220	20.1	7% Imperv	ious Area	
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
11.3	100	0.0900	0.15		Sheet Flow, woods
					Woods: Light underbrush n= 0.400 P2= 3.46"
0.1	46	0.1520	6.28		Shallow Concentrated Flow, Woods
					Unpaved Kv= 16.1 fps
0.2	89	0.1900	7.02		Shallow Concentrated Flow, woods
					Unpaved Kv= 16.1 fps
0.5	174	0.1290	5.78		Shallow Concentrated Flow, Woods
					Unpaved Kv= 16.1 fps
12.1	409	Total	•		

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#### **Subcatchment P1-1: Direct to Wetlands**



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### **Summary for Subcatchment P1-2: To Detention Pond**

Runoff = 11.70 cfs @ 12.22 hrs, Volume= 1.090 af, Depth= 1.60"

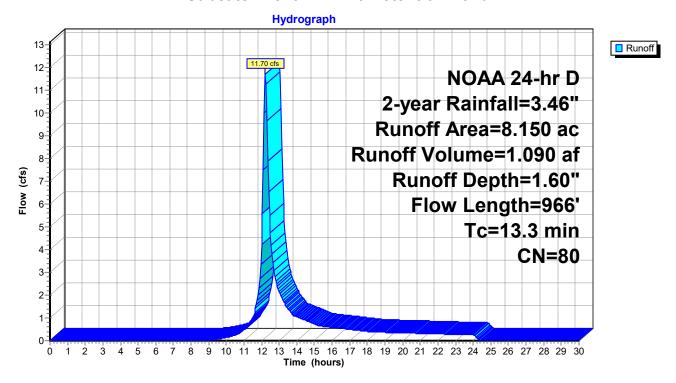
Routed to Pond 2P: Detention Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 2-year Rainfall=3.46"

Area	(ac) C	N Desc	cription				
3.240 70			ds, Good,				
	2.490 74		>75% Grass cover, Good, HSG C				
			Paved parking, HSG C				
		•	Weighted Average				
	730		1% Pervio				
2.	420	29.6	9% Imper	/ious Area			
Тс	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
10.8	100	0.1000	0.15		Sheet Flow, Woods		
					Woods: Light underbrush n= 0.400 P2= 3.46"		
0.8	239	0.0920	4.88		Shallow Concentrated Flow, Woods		
					Unpaved Kv= 16.1 fps		
8.0	179	0.0330	3.69		Shallow Concentrated Flow, Impervious		
					Paved Kv= 20.3 fps		
0.1	48	0.2520	8.08		Shallow Concentrated Flow, Woods		
					Unpaved Kv= 16.1 fps		
0.2	44	0.0400	3.22		Shallow Concentrated Flow, Grass		
0.0	050	0.0000	45.04	40.70	Unpaved Kv= 16.1 fps		
0.3	250	0.0600	15.24	18.70	Pipe Channel, pipe to detention pond		
					15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'		
0.0	400	0.0050	0.40	00.00	n= 0.011 Concrete pipe, straight & clean		
0.3	106	0.0058	6.48	20.36	Pipe Channel, pipe to detention pond		
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'		
40.0					n= 0.011 Concrete pipe, straight & clean		
13.3	966	Total					

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#### **Subcatchment P1-2: To Detention Pond**



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### **Summary for Reach TS: Total Site**

[40] Hint: Not Described (Outflow=Inflow)

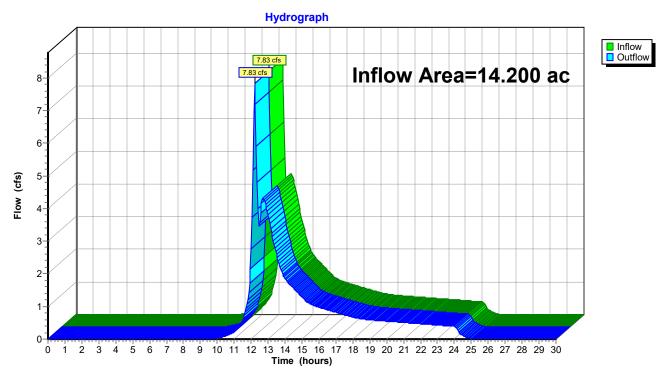
Inflow Area = 14.200 ac, 25.63% Impervious, Inflow Depth = 1.10" for 2-year event

7.83 cfs @ 12.20 hrs, Volume= Inflow 1.301 af

7.83 cfs @ 12.20 hrs, Volume= Outflow 1.301 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

#### **Reach TS: Total Site**



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#### **Summary for Pond 2P: Detention Pond**

Inflow Area = 8.150 ac, 29.69% Impervious, Inflow Depth = 1.60" for 2-year event

Inflow = 11.70 cfs @ 12.22 hrs, Volume= 1.090 af

Outflow = 2.56 cfs @ 12.83 hrs, Volume= 0.664 af, Atten= 78%, Lag= 36.6 min

Discarded = 0.05 cfs @ 12.83 hrs, Volume= 0.070 af Primary = 2.51 cfs @ 12.83 hrs, Volume= 0.595 af

Routed to Reach TS: Total Site

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routed to Reach TS: Total Site

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 256.91' @ 12.83 hrs Surf.Area= 6,899 sf Storage= 22,022 cf

Plug-Flow detention time= 257.8 min calculated for 0.664 af (61% of inflow)

Center-of-Mass det. time= 136.6 min ( 993.0 - 856.4 )

Volume	Inv	ert Ava	il.Storage	Storage	Description		
#1	250.	00'	49,076 cf	Custon	n Stage Data (Pri	smatic) Listed below (Recalc)	
Elevation	an.	Surf.Area	Inc	:Store	Cum.Store		
(fee	_	(sq-ft)		c-feet)	(cubic-feet)		
			(Cubi				
250.0		624		0	0		
251.0	00	1,125		875	875		
252.0	00	1,687		1,406	2,281		
253.0	00	2,459		2,073	4,354		
254.0	00	3,344		2,902	7,255		
255.00		4,361		3,853	11,108		
256.0	00	5,885		5,123	16,231		
257.0	00	7,004		6,445	22,675		
258.0	00	8,170		7,587	30,262		
259.0	00	9,393		8,782	39,044		
260.0	00	10,672	•	10,033	49,076		
Device	Routing	Ir	vert Outl	et Device	es		
#1	Primary	254	4.60' <b>24.0</b>	" Round	174' - 24" HDPE	@ 2.84% Culvert	
	·		L= 7	74.0' RCP, mitered to conform to fill, Ke= 0.700			

Device	Routing	invert	Outlet Devices
#1	Primary	254.60'	24.0" Round 74' - 24" HDPE @ 2.84% Culvert
			L= 74.0' RCP, mitered to conform to fill, Ke= 0.700
			Inlet / Outlet Invert= 254.60' / 252.50' S= 0.0284 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Device 1	256.50'	<b>36.0" W x 10.0" H Vert. Orifice/Grate</b> C= 0.600
			Limited to weir flow at low heads
#3	Device 1	257.60'	<b>40.0" x 33.0" Horiz. Grate</b> C= 0.600
			Limited to weir flow at low heads
#4	Discarded	250.00'	0.210 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 245.00'
#5	Secondary	259.09'	<b>20.8" W x 32.8" H Vert. Emergency Overflow</b> C= 0.600
	•		Limited to weir flow at low heads

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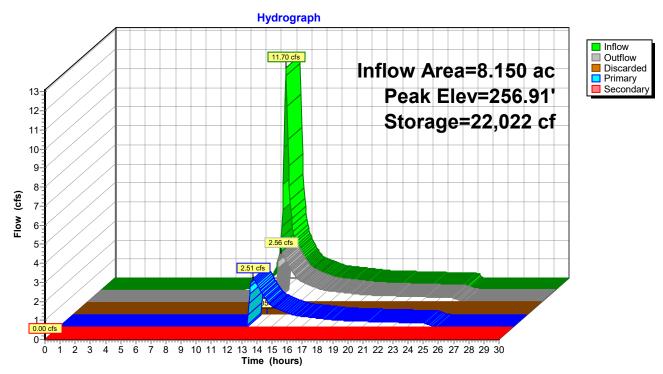
**Discarded OutFlow** Max=0.05 cfs @ 12.83 hrs HW=256.91' (Free Discharge) **4=Exfiltration** (Controls 0.05 cfs)

Primary OutFlow Max=2.49 cfs @ 12.83 hrs HW=256.91' (Free Discharge)
1=74' - 24" HDPE @ 2.84% Culvert (Passes 2.49 cfs of 15.25 cfs potential flow)
2=Orifice/Grate (Orifice Controls 2.49 cfs @ 2.04 fps)
3=Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=250.00' (Free Discharge)

5=Emergency Overflow (Controls 0.00 cfs)

#### **Pond 2P: Detention Pond**



NOAA 24-hr D 10-year Rainfall=5.11"

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Time span=0.00-30.00 hrs, dt=0.05 hrs, 601 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment P1-1: Direct to Wetlands**Runoff Area=6.050 ac 20.17% Impervious Runoff Depth=2.72"
Flow Length=409' Tc=12.1 min CN=77 Runoff=15.36 cfs 1.369 af

**Subcatchment P1-2: To Detention Pond**Runoff Area=8.150 ac 29.69% Impervious Runoff Depth=2.99"
Flow Length=966' Tc=13.3 min CN=80 Runoff=21.83 cfs 2.030 af

Reach TS: Total Site Inflow=25.98 cfs 2.898 af Outflow=25.98 cfs 2.898 af

**Pond 2P: Detention Pond**Peak Elev=257.82' Storage=28,794 cf Inflow=21.83 cfs 2.030 af Discarded=0.06 cfs 0.074 af Primary=15.40 cfs 1.530 af Secondary=0.00 cfs 0.000 af Outflow=15.46 cfs 1.603 af

Total Runoff Area = 14.200 ac Runoff Volume = 3.399 af Average Runoff Depth = 2.87" 74.37% Pervious = 10.560 ac 25.63% Impervious = 3.640 ac

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### **Summary for Subcatchment P1-1: Direct to Wetlands**

Runoff = 15.36 cfs @ 12.20 hrs, Volume= 1.369 af, Depth= 2.72"

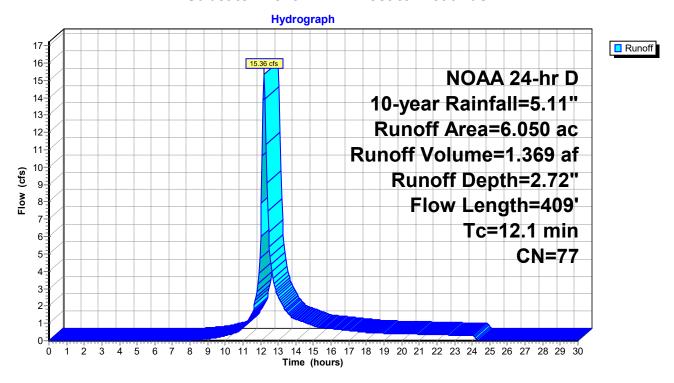
Routed to Reach TS: Total Site

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 10-year Rainfall=5.11"

Area (ac) CN Description								
	2.	680 7	'0 Woo	Woods, Good, HSG C				
	2.	150 7	'4 >75°	>75% Grass cover, Good, HSG C				
	1.220 98 Pa			Paved parking, HSG C				
	6.	050 7	7 Wei	Weighted Average				
		830		3% Pervio				
	1.	220	20.1	7% Imper	ious Area			
	То	Longth	Slope	Volocity	Consoity	Description		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
_	11.3	100	0.0900	0.15	(010)	Sheet Flow, woods		
	11.5	100	0.0300	0.15		Woods: Light underbrush n= 0.400 P2= 3.46"		
	0.1	46	0.1520	6.28		Shallow Concentrated Flow, Woods		
	0	.0	0020	0.20		Unpaved Kv= 16.1 fps		
	0.2	89	0.1900	7.02		Shallow Concentrated Flow, woods		
						Unpaved Kv= 16.1 fps		
	0.5	174	0.1290	5.78		Shallow Concentrated Flow, Woods		
_						Unpaved Kv= 16.1 fps		
	12.1	409	Total					

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#### **Subcatchment P1-1: Direct to Wetlands**



### **Summary for Subcatchment P1-2: To Detention Pond**

[47] Hint: Peak is 117% of capacity of segment #6 [47] Hint: Peak is 107% of capacity of segment #7

Runoff = 21.83 cfs @ 12.21 hrs, Volume= 2.030 af, Depth= 2.99"

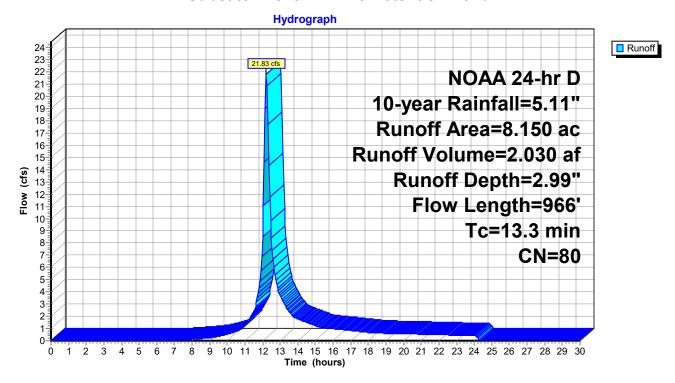
Routed to Pond 2P: Detention Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 10-year Rainfall=5.11"

Area	(ac) C	N Desc	cription		
3.240 70		'0 Woo	ds, Good,	HSG C	
2.	.490 7	4 >75% Grass cover, Good,			, HSG C
2.	.420	8 Pave	ed parking	, HSG C	
8.	.150 8	30 Wei	ghted Avei	rage	
_	.730		1% Pervio		
2.	.420	29.6	9% Imper	vious Area	
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	•
10.8	100	0.1000	0.15		Sheet Flow, Woods
					Woods: Light underbrush n= 0.400 P2= 3.46"
0.8	239	0.0920	4.88		Shallow Concentrated Flow, Woods
					Unpaved Kv= 16.1 fps
0.8	179	0.0330	3.69		Shallow Concentrated Flow, Impervious
					Paved Kv= 20.3 fps
0.1	48	0.2520	8.08		Shallow Concentrated Flow, Woods
0.0	4.4	0.0400	0.00		Unpaved Kv= 16.1 fps
0.2	44	0.0400	3.22		Shallow Concentrated Flow, Grass
0.0	250	0.0000	45.04	40.70	Unpaved Kv= 16.1 fps
0.3	250	0.0600	15.24	18.70	Pipe Channel, pipe to detention pond 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'
					n= 0.011 Concrete pipe, straight & clean
0.3	106	0.0058	6.48	20.36	Pipe Channel, pipe to detention pond
0.5	100	0.0000	0.40	20.50	24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
					n= 0.011 Concrete pipe, straight & clean
13.3	966	Total			11 0.011 Controloto pipo, otraigni a oloan
10.0	900	i Ulai			

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#### **Subcatchment P1-2: To Detention Pond**



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## **Summary for Reach TS: Total Site**

[40] Hint: Not Described (Outflow=Inflow)

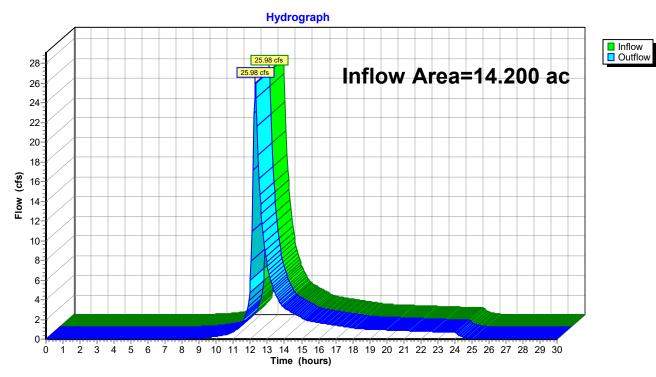
Inflow Area = 14.200 ac, 25.63% Impervious, Inflow Depth = 2.45" for 10-year event

Inflow

14.200 ac, 25.05% impervious, 25.98 cfs @ 12.30 hrs, Volume= 2.898 at 2.898 af, Atten= 0%, Lag= 0.0 min Outflow

Routing by Stor-Ind+Trans method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

## **Reach TS: Total Site**



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## **Summary for Pond 2P: Detention Pond**

Inflow Area = 8.150 ac, 29.69% Impervious, Inflow Depth = 2.99" for 10-year event

Inflow = 21.83 cfs @ 12.21 hrs, Volume= 2.030 af

Outflow = 15.46 cfs @ 12.34 hrs, Volume= 1.603 af, Atten= 29%, Lag= 7.8 min

Discarded = 0.06 cfs @ 12.34 hrs, Volume= 0.074 af Primary = 15.40 cfs @ 12.34 hrs, Volume= 1.530 af

Routed to Reach TS: Total Site

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routed to Reach TS: Total Site

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 257.82' @ 12.34 hrs Surf.Area= 7,958 sf Storage= 28,794 cf

Plug-Flow detention time= 157.0 min calculated for 1.603 af (79% of inflow)

Center-of-Mass det. time= 70.7 min ( 907.2 - 836.6 )

Volume	Invert Ava	il.Storage S	torage D	escription	
#1	250.00'	49,076 cf <b>C</b>	ustom S	tage Data (Pri	smatic) Listed below (Recalc)
Elevation	Surf.Area	Inc.S	tore	Cum.Store	
(feet)	(sq-ft)	(cubic-f	eet)	(cubic-feet)	
250.00	624		0	0	
251.00	1,125		875	875	
252.00	1,687	1,	406	2,281	
253.00	2,459	2,	073	4,354	
254.00	3,344	2,	902	7,255	
255.00	4,361	3,	853	11,108	
256.00	5,885	5,	123	16,231	
257.00	7,004	6,	445	22,675	
258.00	8,170	7,	587	30,262	
259.00	9,393	8,	782	39,044	
260.00	10,672	10,	033	49,076	
Device Ro	outing Ir	nvert Outlet	Devices		

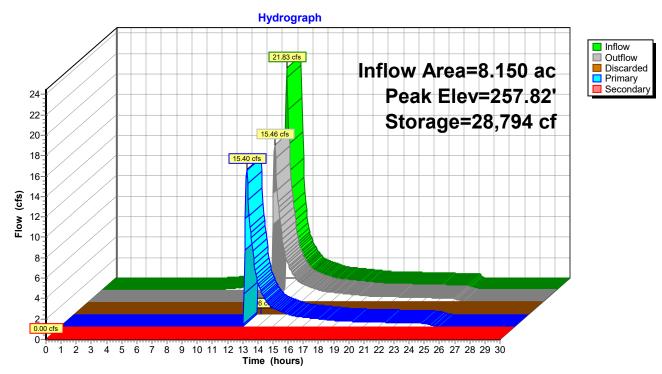
Device	Routing	Invert	Outlet Devices
#1	Primary	254.60'	24.0" Round 74' - 24" HDPE @ 2.84% Culvert
	•		L= 74.0' RCP, mitered to conform to fill, Ke= 0.700
			Inlet / Outlet Invert= 254.60' / 252.50' S= 0.0284 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Device 1	256.50'	<b>36.0" W x 10.0" H Vert. Orifice/Grate</b> C= 0.600
			Limited to weir flow at low heads
#3	Device 1	257.60'	<b>40.0" x 33.0" Horiz. Grate</b> C= 0.600
			Limited to weir flow at low heads
#4	Discarded	250.00'	0.210 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 245.00'
#5	Secondary	259.09'	<b>20.8" W x 32.8" H Vert. Emergency Overflow</b> C= 0.600
	•		Limited to weir flow at low heads

**Discarded OutFlow** Max=0.06 cfs @ 12.34 hrs HW=257.81' (Free Discharge) **4=Exfiltration** (Controls 0.06 cfs)

Primary OutFlow Max=15.24 cfs @ 12.34 hrs HW=257.81' (Free Discharge)
1=74' - 24" HDPE @ 2.84% Culvert (Passes 15.24 cfs of 19.86 cfs potential flow)
2=Orifice/Grate (Orifice Controls 11.30 cfs @ 4.52 fps)
3=Grate (Weir Controls 3.95 cfs @ 1.51 fps)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=250.00' (Free Discharge) **5=Emergency Overflow** ( Controls 0.00 cfs)

### **Pond 2P: Detention Pond**



NOAA 24-hr D 25-year Rainfall=6.15"

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Time span=0.00-30.00 hrs, dt=0.05 hrs, 601 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P1-1: Direct to Wetlands Runoff Area=6.050 ac 20.17% Impervious Runoff Depth=3.61" Flow Length=409' Tc=12.1 min CN=77 Runoff=20.37 cfs 1.820 af

Subcatchment P1-2: To Detention Pond Runoff Area=8.150 ac 29.69% Impervious Runoff Depth=3.92" Flow Length=966' Tc=13.3 min CN=80 Runoff=28.44 cfs 2.660 af

Reach TS: Total Site Inflow=41.15 cfs 3.977 af
Outflow=41.15 cfs 3.977 af

**Pond 2P: Detention Pond**Peak Elev=258.19' Storage=31,873 cf Inflow=28.44 cfs 2.660 af Discarded=0.06 cfs 0.077 af Primary=21.50 cfs 2.157 af Secondary=0.00 cfs 0.000 af Outflow=21.56 cfs 2.233 af

Total Runoff Area = 14.200 ac Runoff Volume = 4.480 af Average Runoff Depth = 3.79" 74.37% Pervious = 10.560 ac 25.63% Impervious = 3.640 ac

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## **Summary for Subcatchment P1-1: Direct to Wetlands**

Runoff = 20.37 cfs @ 12.20 hrs, Volume= 1.820 af, Depth= 3.61"

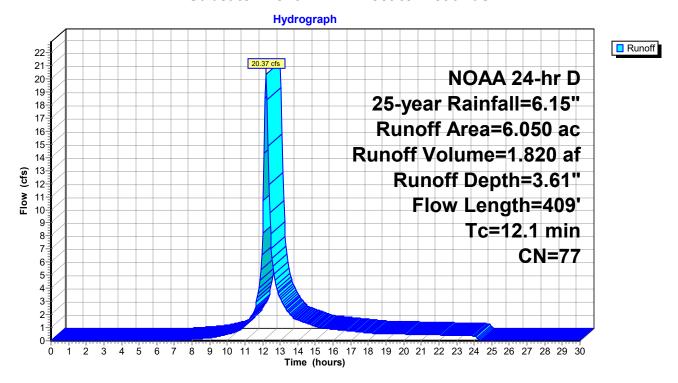
Routed to Reach TS: Total Site

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 25-year Rainfall=6.15"

	Area	(ac) C	N Desc	cription		
2.680 70 Woods, Good, HSG C						
	2.	150 7	'4 >75°	% Grass co	over, Good	, HSG C
	1.	220 9	8 Pave	ed parking	, HSG C	
	6.	050 7	7 Wei	ghted Aver	age	
		830		3% Pervio		
	1.	220	20.1	7% Imper	ious Area	
	То	Longth	Slope	Volocity	Consoity	Description
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	11.3	100	0.0900	0.15	(010)	Sheet Flow, woods
	11.5	100	0.0300	0.15		Woods: Light underbrush n= 0.400 P2= 3.46"
	0.1	46	0.1520	6.28		Shallow Concentrated Flow, Woods
	0	.0	0020	0.20		Unpaved Kv= 16.1 fps
	0.2	89	0.1900	7.02		Shallow Concentrated Flow, woods
						Unpaved Kv= 16.1 fps
	0.5	174	0.1290	5.78		Shallow Concentrated Flow, Woods
_						Unpaved Kv= 16.1 fps
	12.1	409	Total			

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### **Subcatchment P1-1: Direct to Wetlands**



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# **Summary for Subcatchment P1-2: To Detention Pond**

[47] Hint: Peak is 152% of capacity of segment #6 [47] Hint: Peak is 140% of capacity of segment #7

Runoff = 28.44 cfs @ 12.21 hrs, Volume= 2.660 af, Depth= 3.92"

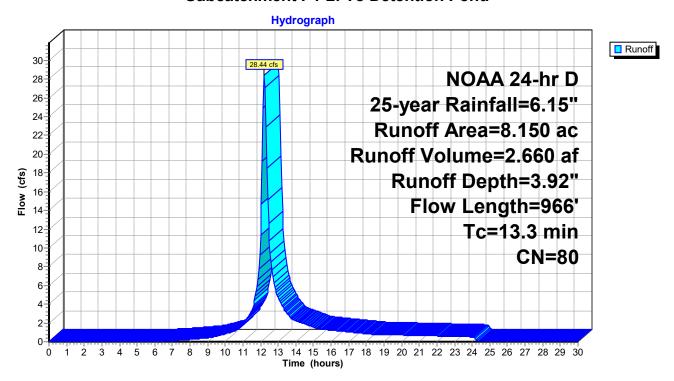
Routed to Pond 2P: Detention Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 25-year Rainfall=6.15"

Area	(ac) C	N Desc	cription		
3.	240 7	'0 Woo	ds, Good,	HSG C	
2.	490 7	'4 >75°	% Grass co	over, Good,	, HSG C
2.	420 9	8 Pave	ed parking	, HSG C	
8.	150 8	80 Weig	ghted Aver	age	
	730		1% Pervio		
2.	420	29.6	9% Imperv	∕ious Area	
_		0.1			<b>D</b>
Tc	Length	Slope	•	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.8	100	0.1000	0.15		Sheet Flow, Woods
0.0	000	0.0000	4.00		Woods: Light underbrush n= 0.400 P2= 3.46"
8.0	239	0.0920	4.88		Shallow Concentrated Flow, Woods
0.8	179	0.0330	3.69		Unpaved Kv= 16.1 fps  Shallow Concentrated Flow, Impervious
0.0	119	0.0330	3.09		Paved Kv= 20.3 fps
0.1	48	0.2520	8.08		Shallow Concentrated Flow, Woods
0.1	10	0.2020	0.00		Unpaved Kv= 16.1 fps
0.2	44	0.0400	3.22		Shallow Concentrated Flow, Grass
					Unpaved Kv= 16.1 fps
0.3	250	0.0600	15.24	18.70	Pipe Channel, pipe to detention pond
					15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'
					n= 0.011 Concrete pipe, straight & clean
0.3	106	0.0058	6.48	20.36	Pipe Channel, pipe to detention pond
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
					n= 0.011 Concrete pipe, straight & clean
13.3	966	Total			

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#### **Subcatchment P1-2: To Detention Pond**



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## **Summary for Reach TS: Total Site**

[40] Hint: Not Described (Outflow=Inflow)

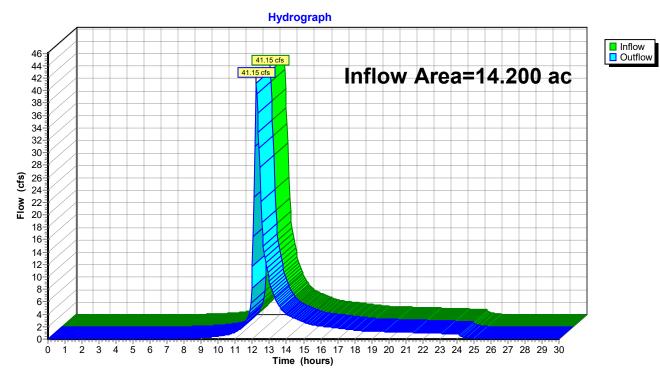
Inflow Area = 14.200 ac, 25.63% Impervious, Inflow Depth = 3.36" for 25-year event

Inflow = 41.15 cfs @ 12.22 hrs, Volume= 3.977 af

Outflow = 41.15 cfs @ 12.22 hrs, Volume= 3.977 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

## **Reach TS: Total Site**



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## **Summary for Pond 2P: Detention Pond**

Inflow Area = 8.150 ac, 29.69% Impervious, Inflow Depth = 3.92" for 25-year event

Inflow = 28.44 cfs @ 12.21 hrs, Volume= 2.660 af

Outflow = 21.56 cfs @ 12.32 hrs, Volume= 2.233 af, Atten= 24%, Lag= 6.3 min

Discarded = 0.06 cfs @ 12.32 hrs, Volume= 0.077 af Primary = 21.50 cfs @ 12.32 hrs, Volume= 2.157 af

Routed to Reach TS: Total Site

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routed to Reach TS: Total Site

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 258.19' @ 12.32 hrs Surf.Area= 8,408 sf Storage= 31,873 cf

Plug-Flow detention time= 130.6 min calculated for 2.233 af (84% of inflow)

Center-of-Mass det. time= 58.3 min ( 886.3 - 828.0 )

Volume	ln۱	vert Ava	il.Storage	Storage	Description	
#1	250.	00'	49,076 cf	Custon	n Stage Data (Pr	ismatic) Listed below (Recalc)
<b>-</b> 1		O	Local	01	0	
Elevation		Surf.Area		c.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubi	c-feet)	(cubic-feet)	
250.0	00	624		0	0	
251.0	00	1,125		875	875	
252.0	00	1,687		1,406	2,281	
253.0	00	2,459		2,073	4,354	
254.0	00	3,344		2,902	7,255	
255.0	00	4,361		3,853	11,108	
256.0	00	5,885		5,123	16,231	
257.0	00	7,004		6,445	22,675	
258.0	00	8,170		7,587	30,262	
259.0	00	9,393		8,782	39,044	
260.0	00	10,672		10,033	49,076	
Device	Routing	lr.	nvert Out	et Device	es	
#1	Primary	25	4.60' <b>24.0</b>	" Round	l 74' - 24" HDPE	@ 2.84% Culvert
			L= 7	'4.0' RC	P. mitered to cor	nform to fill, Ke= 0.700

Device	Rouling	mvert	Outlet Devices
#1	Primary	254.60'	24.0" Round 74' - 24" HDPE @ 2.84% Culvert
	-		L= 74.0' RCP, mitered to conform to fill, Ke= 0.700
			Inlet / Outlet Invert= 254.60' / 252.50' S= 0.0284 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Device 1	256.50'	· · · · · · · · · · · · · · · · · · ·
			Limited to weir flow at low heads
#3	Device 1	257.60'	<b>40.0" x 33.0" Horiz. Grate</b> C= 0.600
			Limited to weir flow at low heads
#4	Discarded	250.00'	0.210 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 245.00'
#5	Secondary	259.09'	<b>20.8" W x 32.8" H Vert. Emergency Overflow</b> C= 0.600
	•		Limited to weir flow at low heads

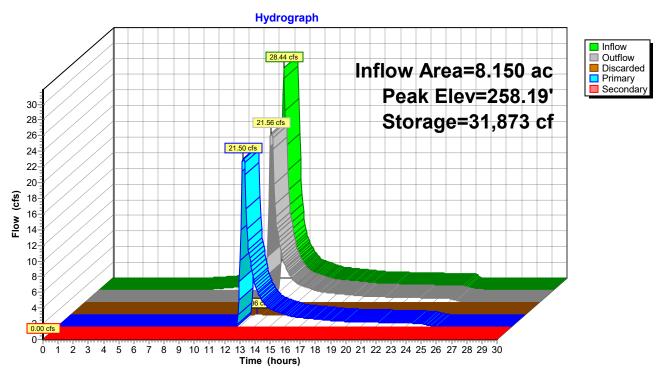
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**Discarded OutFlow** Max=0.06 cfs @ 12.32 hrs HW=258.18' (Free Discharge) **4=Exfiltration** (Controls 0.06 cfs)

Primary OutFlow Max=21.46 cfs @ 12.32 hrs HW=258.18' (Free Discharge)
1=74' - 24" HDPE @ 2.84% Culvert (Inlet Controls 21.46 cfs @ 6.83 fps)
2=Orifice/Grate (Passes < 13.49 cfs potential flow)
3=Grate (Passes < 17.76 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=250.00' (Free Discharge)
5=Emergency Overflow (Controls 0.00 cfs)

**Pond 2P: Detention Pond** 



NOAA 24-hr D 50-year Rainfall=6.92"

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Time span=0.00-30.00 hrs, dt=0.05 hrs, 601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment P1-1: Direct to Wetlands** Runoff Area=6.050 ac 20.17% Impervious Runoff Depth=4.29" Flow Length=409' Tc=12.1 min CN=77 Runoff=24.13 cfs 2.165 af

Subcatchment P1-2: To Detention Pond Runoff Area=8.150 ac 29.69% Impervious Runoff Depth=4.62" Flow Length=966' Tc=13.3 min CN=80 Runoff=33.38 cfs 3.138 af

Reach TS: Total Site Inflow=45.72 cfs 4.797 af Outflow=45.72 cfs 4.797 af

Peak Elev=258.57' Storage=35,115 cf Inflow=33.38 cfs 3.138 af Pond 2P: Detention Pond Discarded=0.07 cfs 0.079 af Primary=23.00 cfs 2.632 af Secondary=0.00 cfs 0.000 af Outflow=23.07 cfs 2.711 af

> Total Runoff Area = 14.200 ac Runoff Volume = 5.303 af Average Runoff Depth = 4.48" 74.37% Pervious = 10.560 ac 25.63% Impervious = 3.640 ac

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## **Summary for Subcatchment P1-1: Direct to Wetlands**

Runoff = 24.13 cfs @ 12.20 hrs, Volume= 2.165 af, Depth= 4.29"

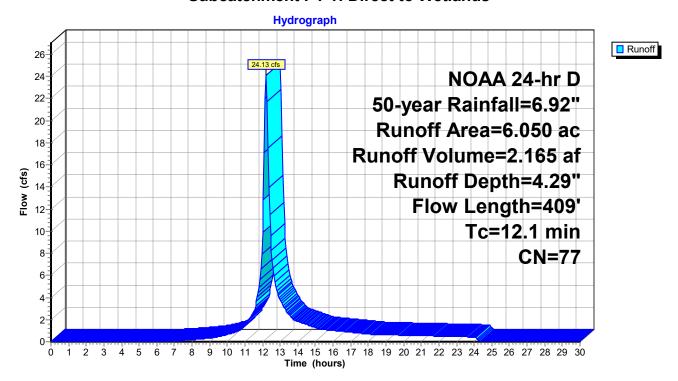
Routed to Reach TS: Total Site

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 50-year Rainfall=6.92"

	Area	(ac) C	N Desc	cription		
2.680 70 Woods, Good, HSG C						
	2.	150 7	'4 >75°	% Grass co	over, Good	, HSG C
	1.	220 9	8 Pave	ed parking	, HSG C	
	6.	050 7	7 Wei	ghted Aver	age	
		830		3% Pervio		
	1.	220	20.1	7% Imper	ious Area	
	То	Longth	Slope	Volocity	Consoity	Description
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	11.3	100	0.0900	0.15	(010)	Sheet Flow, woods
	11.5	100	0.0300	0.15		Woods: Light underbrush n= 0.400 P2= 3.46"
	0.1	46	0.1520	6.28		Shallow Concentrated Flow, Woods
	0	.0	0020	0.20		Unpaved Kv= 16.1 fps
	0.2	89	0.1900	7.02		Shallow Concentrated Flow, woods
						Unpaved Kv= 16.1 fps
	0.5	174	0.1290	5.78		Shallow Concentrated Flow, Woods
_						Unpaved Kv= 16.1 fps
	12.1	409	Total			

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#### **Subcatchment P1-1: Direct to Wetlands**



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## **Summary for Subcatchment P1-2: To Detention Pond**

[47] Hint: Peak is 178% of capacity of segment #6 [47] Hint: Peak is 164% of capacity of segment #7

Runoff = 33.38 cfs @ 12.21 hrs, Volume= 3.138 af, Depth= 4.62"

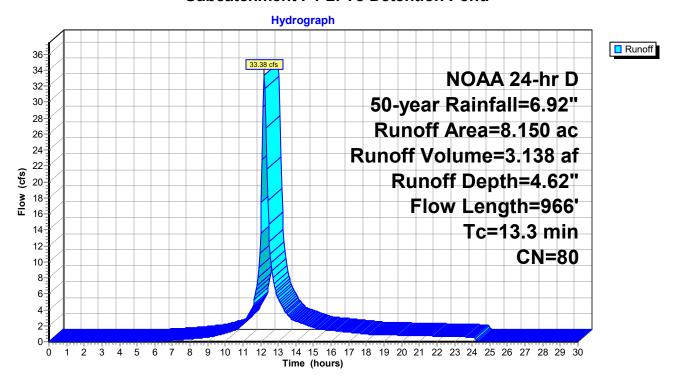
Routed to Pond 2P: Detention Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 50-year Rainfall=6.92"

Area	(ac) C	N Desc	cription		
3.	240 7	'0 Woo	ds, Good,	HSG C	
2.	490 7	'4 >75°	% Grass co	over, Good,	, HSG C
2.	420 9	8 Pave	ed parking	, HSG C	
8.	150 8	80 Weig	ghted Aver	age	
	730		1% Pervio		
2.	420	29.6	9% Imperv	∕ious Area	
_		0.1			<b>D</b>
Tc	Length	Slope	•	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.8	100	0.1000	0.15		Sheet Flow, Woods
0.0	000	0.0000	4.00		Woods: Light underbrush n= 0.400 P2= 3.46"
8.0	239	0.0920	4.88		Shallow Concentrated Flow, Woods
0.8	179	0.0330	3.69		Unpaved Kv= 16.1 fps  Shallow Concentrated Flow, Impervious
0.0	119	0.0330	3.09		Paved Kv= 20.3 fps
0.1	48	0.2520	8.08		Shallow Concentrated Flow, Woods
0.1	10	0.2020	0.00		Unpaved Kv= 16.1 fps
0.2	44	0.0400	3.22		Shallow Concentrated Flow, Grass
					Unpaved Kv= 16.1 fps
0.3	250	0.0600	15.24	18.70	Pipe Channel, pipe to detention pond
					15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'
					n= 0.011 Concrete pipe, straight & clean
0.3	106	0.0058	6.48	20.36	Pipe Channel, pipe to detention pond
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
					n= 0.011 Concrete pipe, straight & clean
13.3	966	Total			

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#### **Subcatchment P1-2: To Detention Pond**



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## **Summary for Reach TS: Total Site**

[40] Hint: Not Described (Outflow=Inflow)

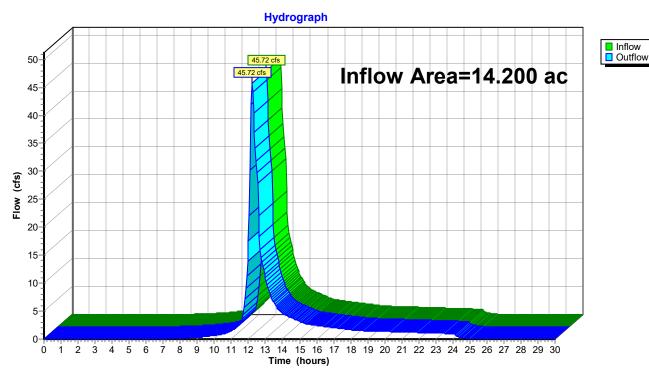
Inflow Area = 14.200 ac, 25.63% Impervious, Inflow Depth = 4.05" for 50-year event

Inflow 4.797 af

45.72 cfs @ 12.21 hrs, Volume= 45.72 cfs @ 12.21 hrs, Volume= Outflow 4.797 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

## **Reach TS: Total Site**



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## **Summary for Pond 2P: Detention Pond**

Inflow Area = 8.150 ac, 29.69% Impervious, Inflow Depth = 4.62" for 50-year event

Inflow = 33.38 cfs @ 12.21 hrs, Volume= 3.138 af

Outflow = 23.07 cfs @ 12.34 hrs, Volume= 2.711 af, Atten= 31%, Lag= 7.6 min

Discarded = 0.07 cfs @ 12.34 hrs, Volume= 0.079 af Primary = 23.00 cfs @ 12.34 hrs, Volume= 2.632 af

Routed to Reach TS: Total Site

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routed to Reach TS: Total Site

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 258.57' @ 12.34 hrs Surf.Area= 8,867 sf Storage= 35,115 cf

Plug-Flow detention time= 116.8 min calculated for 2.707 af (86% of inflow)

Center-of-Mass det. time= 53.4 min (876.1 - 822.8)

Volume	Invert A	Avail.Storage	Storage	Description		
#1	250.00'	49,076 cf	Custom	n Stage Data (Pri	smatic) Listed below (Recalc)	
Elevation	Surf.Ar	00 ln	c.Store	Cum.Store		
(feet)	Suri.Ar		ic-feet)	(cubic-feet)		
		, ,				
250.00		24	0	0		
251.00	1,1:	25	875	875		
252.00	1,6	87	1,406	2,281		
253.00	2,4	59	2,073	4,354		
254.00	3,3	44	2,902	7,255		
255.00	4,3	61	3,853	11,108		
256.00	5,8	85	5,123	16,231		
257.00	7,0	04	6,445	22,675		
258.00	8,1	70	7,587	30,262		
259.00	9,3	93	8,782	39,044		
260.00	10,6	72	10,033	49,076		

Device	Routing	Invert	Outlet Devices
#1	Primary	254.60'	24.0" Round 74' - 24" HDPE @ 2.84% Culvert
			L= 74.0' RCP, mitered to conform to fill, Ke= 0.700
			Inlet / Outlet Invert= 254.60' / 252.50' S= 0.0284 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Device 1	256.50'	<b>36.0" W x 10.0" H Vert. Orifice/Grate</b> C= 0.600
			Limited to weir flow at low heads
#3	Device 1	257.60'	<b>40.0" x 33.0" Horiz. Grate</b> C= 0.600
			Limited to weir flow at low heads
#4	Discarded	250.00'	0.210 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 245.00'
#5	Secondary	259.09'	20.8" W x 32.8" H Vert. Emergency Overflow C= 0.600
			Limited to weir flow at low heads

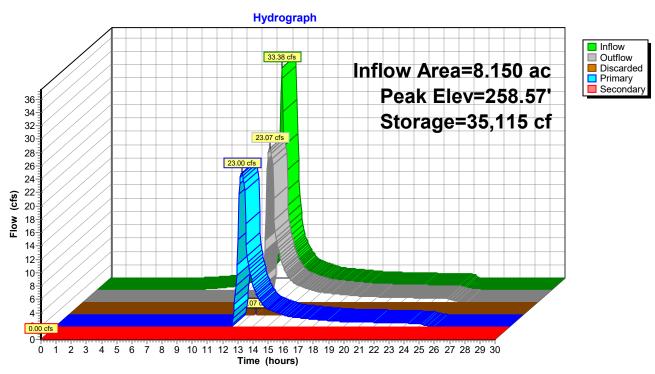
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**Discarded OutFlow** Max=0.07 cfs @ 12.34 hrs HW=258.56' (Free Discharge) **4=Exfiltration** (Controls 0.07 cfs)

Primary OutFlow Max=22.97 cfs @ 12.34 hrs HW=258.56' (Free Discharge)
1=74' - 24" HDPE @ 2.84% Culvert (Inlet Controls 22.97 cfs @ 7.31 fps)
2=Orifice/Grate (Passes < 15.40 cfs potential flow)
3=Grate (Passes < 37.51 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=250.00' (Free Discharge)
5=Emergency Overflow (Controls 0.00 cfs)

**Pond 2P: Detention Pond** 



NOAA 24-hr D 100-year Rainfall=7.74"

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Time span=0.00-30.00 hrs, dt=0.05 hrs, 601 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P1-1: Direct to Wetlands Runoff Area=6.050 ac 20.17% Impervious Runoff Depth=5.04" Flow Length=409' Tc=12.1 min CN=77 Runoff=28.17 cfs 2.539 af

Subcatchment P1-2: To Detention Pond Runoff Area=8.150 ac 29.69% Impervious Runoff Depth=5.38" Flow Length=966' Tc=13.3 min CN=80 Runoff=38.65 cfs 3.655 af

Reach TS: Total Site Inflow=50.73 cfs 5.686 af Outflow=50.73 cfs 5.686 af

**Pond 2P: Detention Pond**Peak Elev=258.99' Storage=38,927 cf Inflow=38.65 cfs 3.655 af Discarded=0.07 cfs 0.081 af Primary=24.57 cfs 3.147 af Secondary=0.00 cfs 0.000 af Outflow=24.64 cfs 3.228 af

Total Runoff Area = 14.200 ac Runoff Volume = 6.194 af Average Runoff Depth = 5.23" 74.37% Pervious = 10.560 ac 25.63% Impervious = 3.640 ac

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## **Summary for Subcatchment P1-1: Direct to Wetlands**

Runoff = 28.17 cfs @ 12.20 hrs, Volume= 2.5

2.539 af, Depth= 5.04"

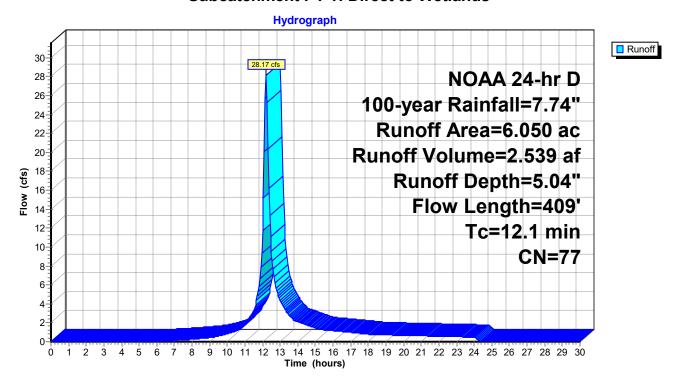
Routed to Reach TS: Total Site

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 100-year Rainfall=7.74"

	Area	(ac) C	N Desc	cription		
2.680 70 Woods, Good, HSG C						
	2.	150 7	'4 >75°	% Grass co	over, Good	, HSG C
	1.	220 9	8 Pave	ed parking	, HSG C	
	6.	050 7	7 Wei	ghted Aver	age	
		830		3% Pervio		
	1.	220	20.1	7% Imper	ious Area	
	То	Longth	Slope	Volocity	Consoity	Description
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	11.3	100	0.0900	0.15	(010)	Sheet Flow, woods
	11.5	100	0.0300	0.15		Woods: Light underbrush n= 0.400 P2= 3.46"
	0.1	46	0.1520	6.28		Shallow Concentrated Flow, Woods
	0	.0	0020	0.20		Unpaved Kv= 16.1 fps
	0.2	89	0.1900	7.02		Shallow Concentrated Flow, woods
						Unpaved Kv= 16.1 fps
	0.5	174	0.1290	5.78		Shallow Concentrated Flow, Woods
_						Unpaved Kv= 16.1 fps
	12.1	409	Total			

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#### **Subcatchment P1-1: Direct to Wetlands**



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# **Summary for Subcatchment P1-2: To Detention Pond**

[47] Hint: Peak is 207% of capacity of segment #6 [47] Hint: Peak is 190% of capacity of segment #7

Runoff = 38.65 cfs @ 12.21 hrs, Volume=

3.655 af, Depth= 5.38"

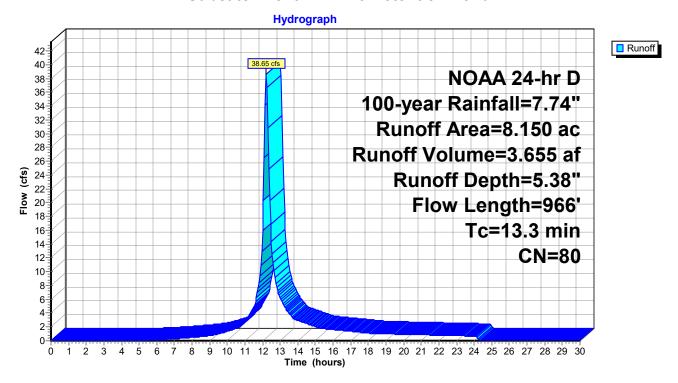
Routed to Pond 2P: Detention Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs NOAA 24-hr D 100-year Rainfall=7.74"

	Area	(ac) C	N Desc	cription		
3.240 70 Woods, Good, HSG C					HSG C	
	2.490 74 >75% Grass cover, Good, I				over, Good	, HSG C
_	2.	420 9	8 Pave	ed parking	, HSG C	
	8.	150 8	0 Wei	ghted Avei	age	
		730		1% Pervio		
	2.	420	29.6	9% Imper\	/ious Area	
	_					
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	10.8	100	0.1000	0.15		Sheet Flow, Woods
						Woods: Light underbrush n= 0.400 P2= 3.46"
	0.8	239	0.0920	4.88		Shallow Concentrated Flow, Woods
		470		0.00		Unpaved Kv= 16.1 fps
	8.0	179	0.0330	3.69		Shallow Concentrated Flow, Impervious
	0.4	40	0.0500	0.00		Paved Kv= 20.3 fps
	0.1	48	0.2520	8.08		Shallow Concentrated Flow, Woods
	0.2	44	0.0400	3.22		Unpaved Kv= 16.1 fps Shallow Concentrated Flow, Grass
	0.2	44	0.0400	3.22		Unpaved Kv= 16.1 fps
	0.3	250	0.0600	15.24	18.70	·
	0.5	230	0.0000	13.24	10.70	15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'
						n= 0.011 Concrete pipe, straight & clean
	0.3	106	0.0058	6.48	20.36	Pipe Channel, pipe to detention pond
	0.0	.00	0.0000	0.70	20.00	24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
						n= 0.011 Concrete pipe, straight & clean
_	13.3	966	Total			1 1 / J -

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### **Subcatchment P1-2: To Detention Pond**



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## **Summary for Reach TS: Total Site**

[40] Hint: Not Described (Outflow=Inflow)

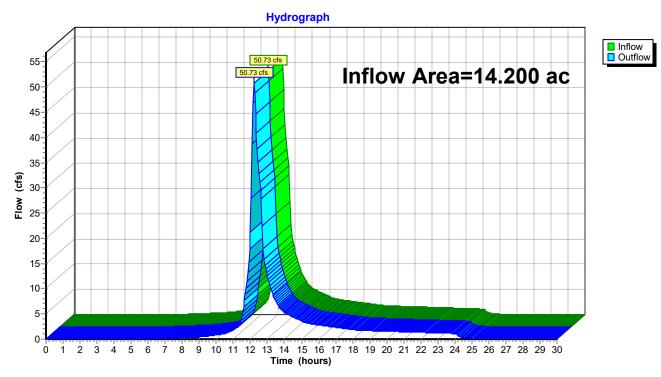
Inflow Area = 14.200 ac, 25.63% Impervious, Inflow Depth = 4.81" for 100-year event

50.73 cfs @ 12.21 hrs, Volume= Inflow 5.686 af

50.73 cfs @ 12.21 hrs, Volume= Outflow 5.686 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

## **Reach TS: Total Site**



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## **Summary for Pond 2P: Detention Pond**

Inflow Area = 8.150 ac, 29.69% Impervious, Inflow Depth = 5.38" for 100-year event
Inflow = 38.65 cfs @ 12.21 hrs, Volume= 3.655 af
Outflow = 24.64 cfs @ 12.36 hrs, Volume= 3.228 af, Atten= 36%, Lag= 8.8 min

Discarded = 0.07 cfs @ 12.36 hrs, Volume= 0.081 af Primary = 24.57 cfs @ 12.36 hrs, Volume= 3.147 af

Routed to Reach TS: Total Site

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routed to Reach TS: Total Site

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 258.99' @ 12.36 hrs Surf.Area= 9,378 sf Storage= 38,927 cf

Plug-Flow detention time= 106.7 min calculated for 3.222 af (88% of inflow)

Center-of-Mass det. time= 49.9 min (867.9 - 818.0)

Volume	In	vert Ava	il.Storage	Storage	Description	
#1	250	0.00'	49,076 cf	Custom	Stage Data (Pris	smatic) Listed below (Recalc)
Elevation	on	Surf.Area	Inc	.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubi	c-feet)	(cubic-feet)	
250.0	00	624		0	0	
251.0	00	1,125		875	875	
252.0	00	1,687		1,406	2,281	
253.0	00	2,459		2,073	4,354	
254.0	00	3,344		2,902	7,255	
255.0	00	4,361		3,853	11,108	
256.	00	5,885		5,123	16,231	
257.	00	7,004		6,445	22,675	
258.0	00	8,170		7,587	30,262	
259.0	00	9,393		8,782	39,044	
260.0	00	10,672		10,033	49,076	
Device	Routing	g Ir	vert Outl	et Devices	5	
#1	Drimar	25.	160' 240	" Pound	74' 24" LIDE	@ 2 84% Culvort

Device	Routing	Invert	Outlet Devices
#1	Primary	254.60'	24.0" Round 74' - 24" HDPE @ 2.84% Culvert
			L= 74.0' RCP, mitered to conform to fill, Ke= 0.700
			Inlet / Outlet Invert= 254.60' / 252.50' S= 0.0284 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Device 1	256.50'	<b>36.0" W x 10.0" H Vert. Orifice/Grate</b> C= 0.600
			Limited to weir flow at low heads
#3	Device 1	257.60'	<b>40.0" x 33.0" Horiz. Grate</b> C= 0.600
			Limited to weir flow at low heads
#4	Discarded	250.00'	0.210 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 245.00'
#5	Secondary	259.09'	<b>20.8" W x 32.8" H Vert. Emergency Overflow</b> C= 0.600
	•		Limited to weir flow at low heads

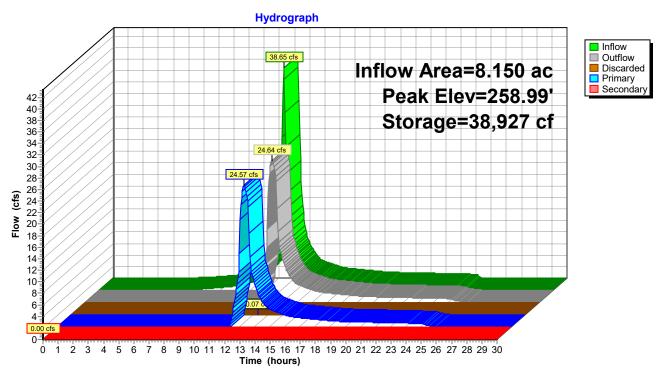
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**Discarded OutFlow** Max=0.07 cfs @ 12.36 hrs HW=258.98' (Free Discharge) **4=Exfiltration** (Controls 0.07 cfs)

Primary OutFlow Max=24.54 cfs @ 12.36 hrs HW=258.98' (Free Discharge)
1=74' - 24" HDPE @ 2.84% Culvert (Inlet Controls 24.54 cfs @ 7.81 fps)
2=Orifice/Grate (Passes < 17.27 cfs potential flow)
3=Grate (Passes < 51.88 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=250.00' (Free Discharge)
5=Emergency Overflow (Controls 0.00 cfs)

**Pond 2P: Detention Pond** 



# **APPENDIX C**

Hydraulic Analysis





§8-30g,

SCALE: 1" = 50'

DRAWN BY: CLM CHECKED BY: WGW

**CATCHMENT** AREA MAP

CAM

Drainage Analysis for Proposed Conditions Ledyard Housing Development Ledyard, CT



*Job Number:* 0725-500010.00

## **Drainage Areas**

DACINI	TOTAL (CE)	TOTAL	IMPERV.	IMPERV.	PERVIOUS	PERVIOUS	CVI	T. (Mr. )
BASIN	TOTAL (SF)	(AC)	(SF)	(AC)	(SF)	(AC)	C-Value	Tc (Min.)
DCCB-101	5,163	0.12	2571	0.06	2,592	0.06	0.60	5.0
DCCB-102	1,743	0.04	1592	0.04	151	0.00	0.85	5.0
DCCB-103	3,501	0.08	2,874	0.07	627	0.01	0.79	5.0
DCCB-104	2,276	0.05	1,786	0.04	490	0.01	0.77	5.0
DCCB-104A	2,328	0.05	1,538	0.04	790	0.02	0.70	5.0
DCCB-105	15,343	0.35	3,498	0.08	11,845	0.27	0.44	15.1
CCB-106	8,566	0.20	3,946	0.09	4,620	0.11	0.58	5.0
CCB-107	7,731	0.18	3,332	0.08	4,398	0.10	0.56	8.8
DCCB-108	23,427	0.54	3,430	0.08	19,996	0.46	0.39	13.0
CCB-109	8,811	0.20	6,121	0.14	2,690	0.06	0.72	13.3
CCB-110	491	0.01	491	0.01	0	0.00	0.90	5.0
CCB-111	4,897	0.11	3,042	0.07	1,855	0.04	0.67	5.0
AD-112	315	0.01	0	0.00	315	0.01	0.30	5.0
AD-113	3,560	0.08	1754.06	0.04	1,805	0.04	0.60	5.0
AD-114	10,063	0.23	3019.5	0.07	7,044	0.16	0.48	5.0
AD-115	13,616	0.31	3979.81	0.09	9,636	0.22	0.48	5.0
AD-116	5,167	0.12	0	0.00	5,167	0.12	0.30	5.0
DCCB-117	10,815	0.25	4189.04	0.10	6,626	0.15	0.53	6.4
DCCB-118	13,632	0.31	6424.95	0.15	7,207	0.17	0.58	7.6
CCB-119	798	0.02	798	0.02	0	0.00	0.90	5.0
CCB-120	15,689	0.36	2860.33	0.07	12,828	0.29	0.41	11.0
CLCB-121	16,351	0.38	0	0.00	16,351	0.38	0.30	11.9
CLCB-122	41,176	0.95	0	0.00	41,176	0.95	0.30	11.8
CCB-123	3,276	0.08	2107.39	0.05	1,168	0.03	0.69	5.0
CCB-124	2,658	0.06	2291.92	0.05	366	0.01	0.82	5.0
DCCB-125	6,289	0.14	3301.43	0.08	2,987	0.07	0.61	5.0
DCCB-126	4,825	0.11	1588.98	0.04	3,236	0.07	0.50	5.0
DCCB - 202	5,375	0.12	4,682	0.11	693	0.02	0.82	5.0
DCCB - 203	7,026	0.16	3,823	0.09	3,203	0.07	0.63	5.0
EX CCB - 205	3,933	0.09	2,319	0.05	1,614	0.04	0.65	5.0
EX CCB-206	6,668	0.15	2,380	0.05	4,288	0.10	0.51	5.0
CCB - 207	2,795	0.06	2,518	0.06	277	0.01	0.84	5.0
CCB-208	3,412	0.08	2,183	0.05	1,229	0.03	0.68	5.0
AD-300	4,439	0.10	2013	0.05	2,426	0.06	0.57	5.0
AD-301	5,695	0.13	0	0.00	5,695	0.13	0.30	9.4

# **Storm Sewer Tabulation**

Statio	n	Len	Drng A	rea	Rnoff	Area x	C	Тс		Rain			Vel	Pipe		Invert Ele	ev	HGL Ele	v	Grnd / Rim Elev		Line ID
Line	То		Incr	Total	coeff	Incr	Total	Inlet	Syst	(I) 	TIOW	full		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	End	106.000	0.12	5.31	0.60	0.07	2.48	5.0	19.8	4.5	11.04	59.26	4.59	24	5.85	256.00	262.20	259.22	263.39	258.00	266.69	DCCB - 101
2	1	23.000	0.04	4.12	0.85	0.03	1.82	5.0	16.5	5.0	9.09	11.38	6.66	18	1.00	262.80	263.03	263.81	264.19	266.69	266.63	DCCB - 102
3	2	64.000	0.08	4.08	0.79	0.06	1.79	5.0	16.3	5.0	8.99	27.28	6.42	18	5.75	263.13	266.81	264.19	267.97	266.63	270.41	DCCB - 103
4	3	137.000	0.05	3.86	0.77	0.04	1.64	5.0	15.8	5.1	8.39	34.03	6.11	18	8.95	266.91	279.17	267.97	280.29	270.41	283.02	DCCB - 104
5	4	81.000	0.05	1.81	0.70	0.04	0.79	5.0	15.4	5.2	4.07	19.98	6.61	15	8.16	279.77	286.38	280.29	287.20	283.02	289.88	DCCB - 104A
6	5	73.000	0.35	1.65	0.44	0.15	0.70	15.1	15.1	5.2	3.64	11.05	5.69	12	8.21	286.48	292.47	287.20	293.28	289.88	296.09	DCCB - 105
7	6	179.000	0.20	0.38	0.58	0.12	0.22	5.0	9.4	6.8	1.47	22.05	3.58	15	9.93	292.84	310.62	293.28	311.10	296.09	314.37	CCB - 106
8	7	22.000	0.18	0.18	0.56	0.10	0.10	8.8	8.8	7.0	0.71	19.27	3.10	15	7.59	310.82	312.49	311.10	312.82	314.37	314.37	CCB - 107
9	6	23.000	0.54	0.92	0.39	0.21	0.32	13.0	13.0	5.7	1.85	7.00	3.10	15	1.00	292.57	292.80	293.28	293.34	296.09	296.04	DCCB - 108
10	1	32.000	0.20	1.07	0.72	0.14	0.58	13.3	19.6	4.5	2.60	19.55	7.56	15	7.81	263.44	265.94	263.75	266.59	266.69	269.29	CCB - 109
11	10	159.000	0.01	0.21	0.90	0.01	0.14	5.0	17.0	4.9	0.68	16.64	2.02	15	5.66	266.04	275.04	266.59	275.36	269.29	278.41	CCB - 110
12	11	59.000	0.11	0.11	0.67	0.07	0.07	5.0	5.0	9.1	0.67	19.74	3.95	15	7.97	275.16	279.86	275.36	280.18	278.41	284.11	CCB - 111
13	11	48.000	0.01	0.01	0.90	0.01	0.01	5.0	5.0	9.1	0.08	18.45	1.09	15	6.96	275.16	278.50	275.36	278.61	278.41	281.75	AD - 112
14	11	31.000	0.08	0.08	0.60	0.05	0.05	5.0	5.0	9.1	0.44	7.00	2.68	15	1.00	275.14	275.45	275.36	275.71	278.41	278.70	AD - 113
15	10	28.000	0.23	0.66	0.48	0.11	0.30	5.0	8.9	7.0	2.06	14.54	3.88	15	4.32	266.04	267.25	266.59	267.82	269.29	270.60	AD - 114
16	15	60.000	0.31	0.43	0.48	0.15	0.18	5.0	8.2	7.3	1.35	15.27	3.24	15	4.77	267.35	270.21	267.82	270.67	270.60	273.56	AD - 115
17	16	51.000	0.12	0.12	0.30	0.04	0.04	5.0	5.0	9.1	0.33	17.36	1.68	15	6.16	270.31	273.45	270.67	273.67	273.56	276.70	AD - 116
18	4	23.000	0.36	2.00	0.52	0.19	0.82	6.4	14.5	5.4	4.39	7.00	4.88	15	1.00	279.42	279.65	280.29	280.50	283.02	283.00	DCCB - 117
19	18	45.000	0.31	1.64	0.58	0.18	0.63	7.6	14.2	5.4	3.42	23.25	4.47	15	11.04	279.75	284.72	280.50	285.47	283.00	288.07	DCCB - 118
20	19	143.000	0.02	1.33	0.90	0.02	0.45	5.0	13.1	5.7	2.56	16.99	4.02	15	5.90	284.82	293.25	285.47	293.89	288.07	296.60	CCB - 119
21	20	32.000	0.36	1.31	0.41	0.15	0.43	11.0	12.9	5.7	2.48	8.57	4.45	15	1.50	293.35	293.83	293.89	294.46	296.60	297.18	CCB - 120
22	9	26.000	0.38	0.38	0.30	0.11	0.11	11.9	11.9	6.0	0.68	7.00	2.24	15	1.00	292.90	293.16	293.34	293.48	296.04	296.59	CLCB - 121
					1									1	1	-						

Number of lines: 24

NOTES:Intensity = 44.54 / (Inlet time + 3.90) ^ 0.73; Return period =Yrs. 25; c = cir e = ellip b = box

Project File: storm - 100.stm

Run Date: 9/3/2025

# **Storm Sewer Tabulation**

Statio	n	Len	Drng A	rea	Rnoff	Area x	C	Тс			Total	Cap full	Vel	Pipe		Invert Ele	ev	HGL Ele	v	Grnd / Rim Elev		Line ID
ine	To		Incr	Total	coeff	Incr	Total	Inlet	Syst	(I)	flow	full		Size	Slope	Dn	Up	Dn	Up	Dn	Up	-
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
00	0.4	00.000	2.05	0.05	2.00	2.00		44.0	44.0		4 70	7.07	0.54	4.5	4.00	200.00	004.05	20.4.40	005.07	007.40	007.00	000 400
23	21	90.000		0.95	0.30	0.29	0.29	11.8	11.8	6.0	1.72	7.07	3.51	15	1.02	293.93	294.85	294.46	295.37	297.18	297.90	CCB - 122
24	3	20.000	0.14	0.14	0.61	0.09	0.09	5.0	5.0	9.1	0.78	7.00	1.80	15	1.00	267.02	267.22	267.97	267.56	270.41	270.47	DCCB - 125
'roje	ect File:	: storm -	100.stn	า												Number	of lines: 2	24		Run Da	te: 9/3/202	25

NOTES:Intensity = 44.54 / (Inlet time + 3.90) ^ 0.73; Return period =Yrs. 25; c = cir e = ellip b = box

# **Storm Sewer Tabulation**

Statio	n	Len	Drng A	rea	Rnoff	Area x	С	Тс		Rain Total			Vel	Pipe		Invert El	ev	HGL Ele	v	Grnd / Rim Elev		Line ID
Line		-	Incr	Total	coeff	Incr	Total	Inlet	Syst	(1)	flow	full		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1		217.000		0.66	0.00	0.00	0.44	0.0	13.0	5.7	17.23	77.52	6.85	24	10.01	224.49	246.21	225.98	247.70	228.70	257.85	MH-201
2		28.000		0.28	0.82	0.10	0.20	5.0	5.5	8.7	1.74	24.50	3.86	24	1.00	253.40	253.68	253.76	254.14	257.85	257.25	DCCB - 202
3		22.000		0.16	0.63	0.10	0.10	5.0	5.0	9.1	0.92	7.00	3.06	15	1.00	253.78	254.00	254.14	254.38	257.25	257.25	DCCB-203
4	1	69.000	0.00	0.38	0.00	0.00	0.24	0.0	11.2	6.2	1.49	58.92	5.52	24	5.78	249.22	253.21	249.44	253.63	257.85	260.14	MH - 204
5	4	113.000	0.09	0.24	0.65	0.06	0.14	5.0	6.3	8.3	1.11	58.95	2.59	24	5.79	253.21	259.75	253.63	260.11	260.14	265.95	EX CCB - 205
6	5	43.000	0.15	0.15	0.51	0.08	0.08	5.0	5.0	9.1	0.70	6.66	3.12	15	0.91	260.30	260.69	260.57	261.02	265.95	265.90	EX CCB - 206
7	4	10.000	0.06	0.06	0.84	0.05	0.05	5.0	5.0	9.1	0.46	0.00	2.83	15	1.00	256.55	256.65	256.77	256.91	260.14	259.90	CCB - 207
8	4	7.000	0.08	0.08	0.68	0.05	0.05	5.0	5.0	9.1	0.49	0.00	2.89	15	1.00	256.56	256.63	256.79	256.90	260.14	259.88	CCB - 208
9	1	74.000	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	14.72	0.00	9.62	24	3.42	254.47	257.00	255.25	258.38	257.85	257.90	OCS - 1

Number of lines: 9

NOTES:Intensity = 44.54 / (Inlet time + 3.90) ^ 0.73; Return period =Yrs. 25; c = cir e = ellip b = box

Project File: storm - 200.stm

Run Date: 9/4/2025

## **Storm Sewer Tabulation**

Statio	n	Len	Drng A	rea	Rnoff	Area x	C	Тс			Total	Сар	Vel	Pipe		Invert El	ev	HGL Ele	v	Grnd / Ri	m Elev	Line ID
ine	То		Incr	Total	coeff	Incr	Total	Inlet	Syst	(I)	flow	full		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	End	69.000	0.10	0.39	0.57	0.06	0.14	5.0	16.1	5.0	0.71	16.09	2.75	15	5.29	272.50	276.15	272.83	276.48	273.75	279.50	AD-300
2		40.000		0.29	0.30	0.04	0.09	9.4	14.5	5.2	0.46	7.82	2.69	15	1.25	276.25	276.75	276.48	277.01	279.50	280.10	AD-301
3	2	49.000	0.16	0.16	0.30	0.05	0.05	11.1	11.1	6.1	0.29	0.00	2.63	15	9.39	276.85	281.45	277.01	281.66	280.10	284.70	AD-302

Number of lines: 3

NOTES:Intensity = 38.62 / (Inlet time + 3.60) ^ 0.69; Return period =Yrs. 25; c = cir e = ellip b = box

Project File: storm - 300.stm

Run Date: 8/29/2025

## **APPENDIX D**

Water Quality Volume



	Water Quality Volume Computations 8, 9, 11 Colby Drive, Ledyard, CT Project # 0725-500010.00									
Designation	Description	Total Area (ac)	Total Impervious Area (ac)	Impervious Coverage, I (%)	- ( )	WQV (ac-ft, apply 1.3")	Required WQV (cf)	Provided WQV (cf)		
			(,	(73)	R = 0.05 + 0.009*(I)	WQV = (1.3")*(R)*(A)/12	(-1)			
1	Total Site	14.19	3.63	25.59	0.28	0.431	18,774	19,888		
2	Flow to Pond	8.15	2.42	29.65	0.32	0.280	12,183	19,888		

# **APPENDIX E**

NOAA Rainfall Data





#### NOAA Atlas 14, Volume 10, Version 3 Location name: Ledyard, Connecticut, USA\* Latitude: 41.4421°, Longitude: -72.0096° Elevation: 269 ft\*\*

\* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### PF tabular

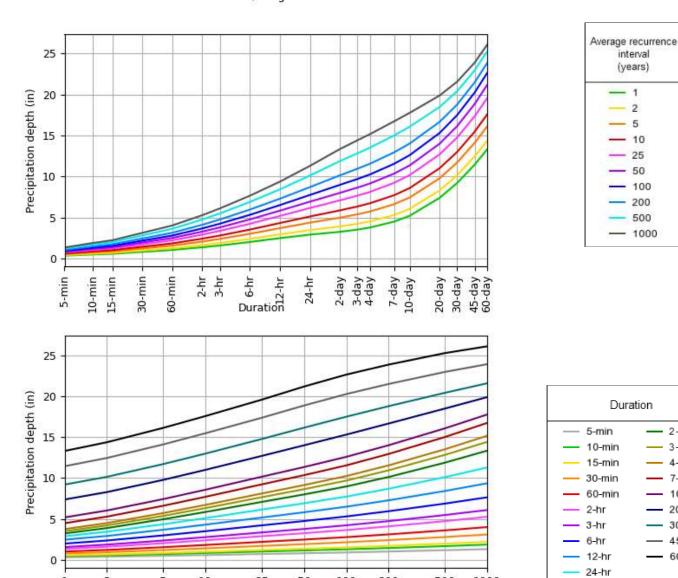
PDS-	based poi	nt precipi	itation fre	quency es	stimates v	/ith 90%	confiden	ce interv	als (in in	ches) <sup>1</sup>
Duration				Average	recurrence	interval (ye	ears)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	<b>0.341</b> (0.264-0.437)	<b>0.408</b> (0.315-0.523)	<b>0.517</b> (0.399-0.665)	<b>0.607</b> (0.466-0.783)	<b>0.732</b> (0.545-0.975)	<b>0.826</b> (0.602-1.12)	<b>0.925</b> (0.656-1.28)	<b>1.04</b> (0.697-1.45)	<b>1.20</b> (0.776-1.72)	<b>1.33</b> (0.842-1.94)
10-min	<b>0.483</b> (0.374-0.619)	<b>0.577</b> (0.447-0.741)	<b>0.732</b> (0.565-0.942)	<b>0.861</b> (0.660-1.11)	<b>1.04</b> (0.772-1.38)	<b>1.17</b> (0.854-1.58)	<b>1.31</b> (0.930-1.82)	<b>1.47</b> (0.987-2.06)	<b>1.70</b> (1.10-2.43)	<b>1.88</b> (1.19-2.74)
15-min	<b>0.568</b> (0.440-0.728)	<b>0.679</b> (0.526-0.872)	<b>0.861</b> (0.664-1.11)	<b>1.01</b> (0.777-1.31)	<b>1.22</b> (0.908-1.62)	<b>1.38</b> (1.00-1.86)	<b>1.54</b> (1.09-2.14)	<b>1.73</b> (1.16-2.42)	<b>2.00</b> (1.29-2.86)	<b>2.22</b> (1.40-3.23)
30-min	<b>0.801</b> (0.621-1.03)	<b>0.957</b> (0.741-1.23)	<b>1.21</b> (0.936-1.56)	<b>1.42</b> (1.09-1.84)	<b>1.72</b> (1.28-2.28)	<b>1.94</b> (1.41-2.62)	<b>2.17</b> (1.54-3.01)	<b>2.43</b> (1.63-3.40)	<b>2.81</b> (1.82-4.03)	<b>3.12</b> (1.97-4.54)
60-min	<b>1.03</b> (0.801-1.33)	<b>1.24</b> (0.956-1.58)	<b>1.56</b> (1.21-2.01)	<b>1.84</b> (1.41-2.37)	<b>2.21</b> (1.65-2.95)	<b>2.50</b> (1.82-3.37)	<b>2.79</b> (1.98-3.88)	<b>3.13</b> (2.10-4.39)	<b>3.62</b> (2.34-5.19)	<b>4.02</b> (2.54-5.85)
2-hr	<b>1.36</b> (1.06-1.73)	<b>1.62</b> (1.27-2.06)	<b>2.05</b> (1.60-2.62)	<b>2.41</b> (1.86-3.08)	<b>2.90</b> (2.18-3.83)	<b>3.27</b> (2.40-4.39)	<b>3.66</b> (2.62-5.04)	<b>4.10</b> (2.78-5.71)	<b>4.75</b> (3.09-6.76)	<b>5.28</b> (3.35-7.62)
3-hr	<b>1.58</b> (1.24-1.99)	<b>1.88</b> (1.48-2.38)	<b>2.38</b> (1.86-3.02)	<b>2.79</b> (2.17-3.56)	<b>3.36</b> (2.53-4.42)	3.79 (2.80-5.05)	<b>4.24</b> (3.04-5.81)	<b>4.75</b> (3.22-6.57)	<b>5.49</b> (3.58-7.78)	<b>6.10</b> (3.89-8.78)
6-hr	<b>2.00</b> (1.59-2.51)	<b>2.38</b> (1.89-2.99)	<b>3.00</b> (2.37-3.77)	<b>3.52</b> (2.76-4.44)	<b>4.23</b> (3.21-5.50)	<b>4.76</b> (3.54-6.29)	<b>5.32</b> (3.84-7.23)	<b>5.96</b> (4.07-8.18)	<b>6.89</b> (4.52-9.69)	<b>7.65</b> (4.90-10.9)
12-hr	<b>2.48</b> (1.98-3.08)	<b>2.94</b> (2.34-3.65)	<b>3.69</b> (2.94-4.60)	<b>4.32</b> (3.41-5.40)	<b>5.18</b> (3.96-6.69)	<b>5.82</b> (4.36-7.64)	<b>6.51</b> (4.73-8.78)	<b>7.29</b> (5.00-9.93)	<b>8.42</b> (5.56-11.8)	<b>9.37</b> (6.03-13.3)
24-hr	<b>2.90</b> (2.34-3.57)	<b>3.46</b> (2.78-4.26)	<b>4.36</b> (3.50-5.38)	<b>5.11</b> (4.08-6.34)	<b>6.15</b> (4.74-7.88)	<b>6.92</b> (5.23-9.02)	<b>7.74</b> (5.68-10.4)	<b>8.70</b> (6.01-11.8)	<b>10.1</b> (6.70-14.0)	<b>11.3</b> (7.30-15.9)
2-day	<b>3.24</b> (2.64-3.96)	<b>3.90</b> (3.17-4.76)	<b>4.97</b> (4.03-6.08)	<b>5.86</b> (4.72-7.20)	<b>7.09</b> (5.52-9.02)	<b>8.00</b> (6.10-10.4)	<b>8.98</b> (6.65-12.0)	<b>10.1</b> (7.04-13.6)	<b>11.9</b> (7.91-16.3)	<b>13.3</b> (8.67-18.6)
3-day	<b>3.52</b> (2.88-4.26)	<b>4.22</b> (3.45-5.12)	<b>5.38</b> (4.38-6.54)	<b>6.34</b> (5.13-7.74)	<b>7.66</b> (5.99-9.70)	<b>8.64</b> (6.62-11.1)	<b>9.70</b> (7.21-12.9)	<b>10.9</b> (7.63-14.6)	<b>12.8</b> (8.57-17.6)	<b>14.4</b> (9.39-20.0)
4-day	<b>3.77</b> (3.10-4.56)	<b>4.51</b> (3.70-5.46)	<b>5.72</b> (4.68-6.94)	<b>6.73</b> (5.46-8.19)	<b>8.11</b> (6.37-10.2)	<b>9.14</b> (7.02-11.7)	<b>10.2</b> (7.64-13.6)	<b>11.6</b> (8.07-15.4)	<b>13.5</b> (9.05-18.4)	<b>15.2</b> (9.90-21.0)
7-day	<b>4.49</b> (3.71-5.38)	<b>5.30</b> (4.38-6.36)	<b>6.62</b> (5.45-7.96)	<b>7.72</b> (6.31-9.32)	<b>9.22</b> (7.28-11.5)	<b>10.4</b> (7.99-13.2)	<b>11.6</b> (8.64-15.1)	<b>12.9</b> (9.09-17.1)	<b>15.0</b> (10.1-20.4)	<b>16.7</b> (11.0-23.0)
10-day	<b>5.20</b> (4.32-6.21)	<b>6.05</b> (5.02-7.22)	<b>7.43</b> (6.14-8.90)	<b>8.58</b> (7.05-10.3)	<b>10.2</b> (8.05-12.6)	<b>11.3</b> (8.78-14.3)	<b>12.6</b> (9.43-16.4)	<b>14.0</b> (9.88-18.4)	<b>16.1</b> (10.8-21.7)	<b>17.8</b> (11.7-24.3)
20-day	<b>7.39</b> (6.20-8.73)	<b>8.29</b> (6.95-9.81)	<b>9.78</b> (8.16-11.6)	<b>11.0</b> (9.12-13.1)	<b>12.7</b> (10.1-15.5)	<b>14.0</b> (10.9-17.4)	<b>15.3</b> (11.4-19.5)	<b>16.7</b> (11.8-21.7)	<b>18.5</b> (12.6-24.7)	<b>19.9</b> (13.1-27.0)
30-day	<b>9.20</b> (7.76-10.8)	<b>10.2</b> (8.55-11.9)	<b>11.7</b> (9.82-13.8)	<b>13.0</b> (10.8-15.4)	<b>14.8</b> (11.8-17.9)	<b>16.1</b> (12.6-19.9)	<b>17.5</b> (13.1-22.0)	<b>18.8</b> (13.4-24.3)	<b>20.4</b> (13.9-27.2)	<b>21.6</b> (14.3-29.2)
45-day	<b>11.4</b> (9.71-13.4)	<b>12.5</b> (10.6-14.6)	<b>14.1</b> (11.9-16.5)	<b>15.5</b> (13.0-18.2)	<b>17.4</b> (14.0-20.9)	<b>18.9</b> (14.7-23.0)	<b>20.3</b> (15.1-25.2)	<b>21.5</b> (15.4-27.7)	<b>23.0</b> (15.7-30.4)	<b>23.9</b> (15.9-32.2)
60-day	<b>13.3</b> (11.3-15.5)	<b>14.4</b> (12.2-16.8)	<b>16.1</b> (13.7-18.8)	<b>17.6</b> (14.8-20.6)	<b>19.6</b> (15.8-23.4)	<b>21.2</b> (16.6-25.7)	<b>22.6</b> (16.9-28.0)	<b>23.9</b> (17.2-30.6)	<b>25.3</b> (17.4-33.3)	<b>26.1</b> (17.4-35.0)

<sup>&</sup>lt;sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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#### PDS-based depth-duration-frequency (DDF) curves Latitude: 41.4421°, Longitude: -72.0096°



NOAA Atlas 14, Volume 10, Version 3

10

25

Average recurrence interval (years)

50

Created (GMT): Tue Aug 6 12:45:53 2024

500

1000

2-day

3-day 4-day

7-day 10-day

20-day

30-day

45-day

- 60-day

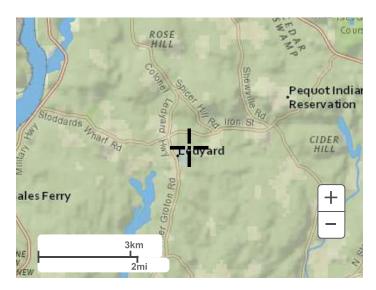
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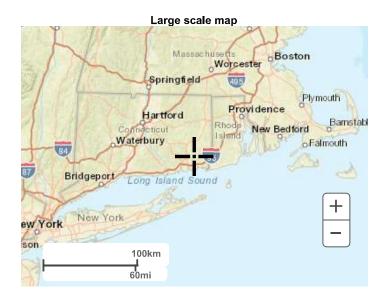
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#### Maps & aerials

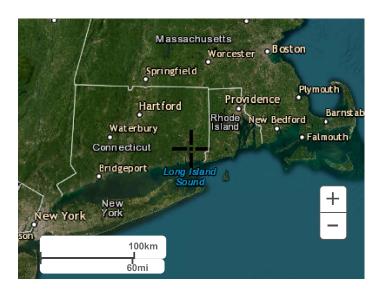
Small scale terrain







Large scale aerial



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Questions?: HDSC.Questions@noaa.gov

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#### NOAA Atlas 14, Volume 10, Version 3 Location name: Ledyard, Connecticut, USA\* Latitude: 41.4421°, Longitude: -72.0096° Elevation: 269 ft\*\*

\* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### PF tabular

PDS-b	ased poir	nt precipit	ation freq	uency es	timates w	ith 90% co	onfidence	intervals	(in inche	s/hour) <sup>1</sup>
Duration				Avera	ge recurren	ce interval (	years)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	<b>4.09</b> (3.17-5.24)	<b>4.90</b> (3.78-6.28)	<b>6.20</b> (4.79-7.98)	<b>7.28</b> (5.59-9.40)	<b>8.78</b> (6.54-11.7)	<b>9.91</b> (7.22-13.4)	<b>11.1</b> (7.87-15.4)	<b>12.4</b> (8.36-17.4)	<b>14.4</b> (9.31-20.6)	<b>16.0</b> (10.1-23.2)
10-min	<b>2.90</b> (2.24-3.71)	<b>3.46</b> (2.68-4.45)	<b>4.39</b> (3.39-5.65)	<b>5.17</b> (3.96-6.67)	<b>6.23</b> (4.63-8.29)	<b>7.03</b> (5.12-9.49)	<b>7.86</b> (5.58-10.9)	<b>8.81</b> (5.92-12.3)	<b>10.2</b> (6.59-14.6)	<b>11.3</b> (7.16-16.5)
15-min	<b>2.27</b> (1.76-2.91)	<b>2.72</b> (2.10-3.49)	<b>3.44</b> (2.66-4.43)	<b>4.05</b> (3.11-5.22)	<b>4.88</b> (3.63-6.50)	<b>5.51</b> (4.02-7.44)	<b>6.17</b> (4.38-8.56)	<b>6.91</b> (4.65-9.68)	<b>7.98</b> (5.17-11.5)	<b>8.87</b> (5.61-12.9)
30-min	<b>1.60</b> (1.24-2.05)	<b>1.91</b> (1.48-2.46)	<b>2.43</b> (1.87-3.12)	<b>2.85</b> (2.19-3.68)	<b>3.43</b> (2.55-4.57)	3.87 (2.82-5.23)	<b>4.33</b> (3.08-6.01)	<b>4.86</b> (3.27-6.81)	<b>5.61</b> (3.64-8.06)	<b>6.24</b> (3.95-9.07)
60-min	<b>1.03</b> (0.801-1.33)	<b>1.24</b> (0.956-1.58)	<b>1.56</b> (1.21-2.01)	<b>1.84</b> (1.41-2.37)	<b>2.21</b> (1.65-2.95)	<b>2.50</b> (1.82-3.37)	<b>2.79</b> (1.98-3.88)	<b>3.13</b> (2.10-4.39)	<b>3.62</b> (2.34-5.19)	<b>4.02</b> (2.54-5.85)
2-hr	<b>0.679</b> (0.531-0.863)	<b>0.811</b> (0.633-1.03)	<b>1.03</b> (0.798-1.31)	<b>1.20</b> (0.932-1.54)	<b>1.45</b> (1.09-1.92)	<b>1.64</b> (1.20-2.19)	<b>1.83</b> (1.31-2.52)	<b>2.05</b> (1.39-2.85)	<b>2.37</b> (1.54-3.38)	<b>2.64</b> (1.68-3.81)
3-hr	<b>0.525</b> (0.412-0.664)	<b>0.626</b> (0.491-0.792)	<b>0.792</b> (0.619-1.00)	<b>0.930</b> (0.722-1.18)	<b>1.12</b> (0.842-1.47)	<b>1.26</b> (0.931-1.68)	<b>1.41</b> (1.01-1.93)	<b>1.58</b> (1.07-2.19)	<b>1.83</b> (1.19-2.59)	<b>2.03</b> (1.30-2.92)
6-hr	<b>0.334</b> (0.265-0.419)	<b>0.397</b> (0.314-0.498)	<b>0.501</b> (0.395-0.630)	<b>0.587</b> (0.460-0.741)	<b>0.705</b> (0.535-0.919)	<b>0.794</b> (0.590-1.05)	<b>0.888</b> (0.641-1.21)	<b>0.994</b> (0.679-1.37)	<b>1.15</b> (0.754-1.62)	<b>1.28</b> (0.818-1.82)
12-hr	<b>0.205</b> (0.164-0.255)	<b>0.243</b> (0.194-0.303)	<b>0.306</b> (0.243-0.381)	<b>0.358</b> (0.283-0.448)	<b>0.429</b> (0.328-0.555)	<b>0.483</b> (0.362-0.634)	<b>0.539</b> (0.392-0.728)	<b>0.604</b> (0.415-0.824)	<b>0.699</b> (0.461-0.976)	<b>0.777</b> (0.500-1.10)
24-hr	<b>0.120</b> (0.097-0.148)	<b>0.143</b> (0.115-0.177)	<b>0.181</b> (0.145-0.224)	<b>0.213</b> (0.169-0.264)	<b>0.256</b> (0.197-0.328)	<b>0.288</b> (0.217-0.375)	<b>0.322</b> (0.236-0.432)	<b>0.362</b> (0.250-0.490)	<b>0.421</b> (0.279-0.584)	<b>0.470</b> (0.304-0.661)
2-day	<b>0.067</b> (0.054-0.082)	<b>0.081</b> (0.066-0.099)	<b>0.103</b> (0.083-0.126)	<b>0.122</b> (0.098-0.149)	<b>0.147</b> (0.114-0.187)	<b>0.166</b> (0.127-0.215)	<b>0.187</b> (0.138-0.249)	<b>0.211</b> (0.146-0.283)	<b>0.247</b> (0.164-0.340)	<b>0.278</b> (0.180-0.388)
3-day	<b>0.048</b> (0.039-0.059)	<b>0.058</b> (0.047-0.071)	<b>0.074</b> (0.060-0.090)	<b>0.088</b> (0.071-0.107)	<b>0.106</b> (0.083-0.134)	<b>0.120</b> (0.091-0.154)	<b>0.134</b> (0.100-0.178)	<b>0.152</b> (0.105-0.203)	<b>0.178</b> (0.119-0.243)	<b>0.200</b> (0.130-0.278)
4-day	<b>0.039</b> (0.032-0.047)	<b>0.047</b> (0.038-0.056)	<b>0.059</b> (0.048-0.072)	<b>0.070</b> (0.056-0.085)	<b>0.084</b> (0.066-0.106)	<b>0.095</b> (0.073-0.122)	<b>0.106</b> (0.079-0.141)	<b>0.120</b> (0.084-0.160)	<b>0.140</b> (0.094-0.192)	<b>0.157</b> (0.103-0.218)
7-day	<b>0.026</b> (0.022-0.032)	<b>0.031</b> (0.026-0.037)	<b>0.039</b> (0.032-0.047)	<b>0.045</b> (0.037-0.055)	<b>0.054</b> (0.043-0.068)	<b>0.061</b> (0.047-0.078)	<b>0.068</b> (0.051-0.090)	<b>0.077</b> (0.054-0.101)	<b>0.089</b> (0.060-0.121)	<b>0.099</b> (0.065-0.137)
10-day	<b>0.021</b> (0.018-0.025)	<b>0.025</b> (0.020-0.030)	<b>0.030</b> (0.025-0.037)	<b>0.035</b> (0.029-0.042)	<b>0.042</b> (0.033-0.052)	<b>0.047</b> (0.036-0.059)	<b>0.052</b> (0.039-0.068)	<b>0.058</b> (0.041-0.076)	<b>0.066</b> (0.045-0.090)	<b>0.074</b> (0.048-0.101)
20-day	<b>0.015</b> (0.012-0.018)	<b>0.017</b> (0.014-0.020)	<b>0.020</b> (0.016-0.024)	<b>0.022</b> (0.019-0.027)	<b>0.026</b> (0.021-0.032)	<b>0.029</b> (0.022-0.036)	<b>0.031</b> (0.023-0.040)	<b>0.034</b> (0.024-0.045)	<b>0.038</b> (0.026-0.051)	<b>0.041</b> (0.027-0.056)
30-day	<b>0.012</b> (0.010-0.015)	<b>0.014</b> (0.011-0.016)	<b>0.016</b> (0.013-0.019)	<b>0.018</b> (0.015-0.021)	<b>0.020</b> (0.016-0.024)	<b>0.022</b> (0.017-0.027)	<b>0.024</b> (0.018-0.030)	<b>0.026</b> (0.018-0.033)	<b>0.028</b> (0.019-0.037)	<b>0.029</b> (0.019-0.040)
45-day	<b>0.010</b> (0.008-0.012)	<b>0.011</b> (0.009-0.013)	<b>0.013</b> (0.011-0.015)	<b>0.014</b> (0.012-0.016)	<b>0.016</b> (0.012-0.019)	<b>0.017</b> (0.013-0.021)	<b>0.018</b> (0.014-0.023)	<b>0.019</b> (0.014-0.025)	<b>0.021</b> (0.014-0.028)	<b>0.022</b> (0.014-0.029)
60-day	<b>0.009</b> (0.007-0.010)	<b>0.009</b> (0.008-0.011)	<b>0.011</b> (0.009-0.013)	<b>0.012</b> (0.010-0.014)	<b>0.013</b> (0.010-0.016)	<b>0.014</b> (0.011-0.017)	<b>0.015</b> (0.011-0.019)	<b>0.016</b> (0.011-0.021)	<b>0.017</b> (0.012-0.023)	<b>0.018</b> (0.012-0.024)

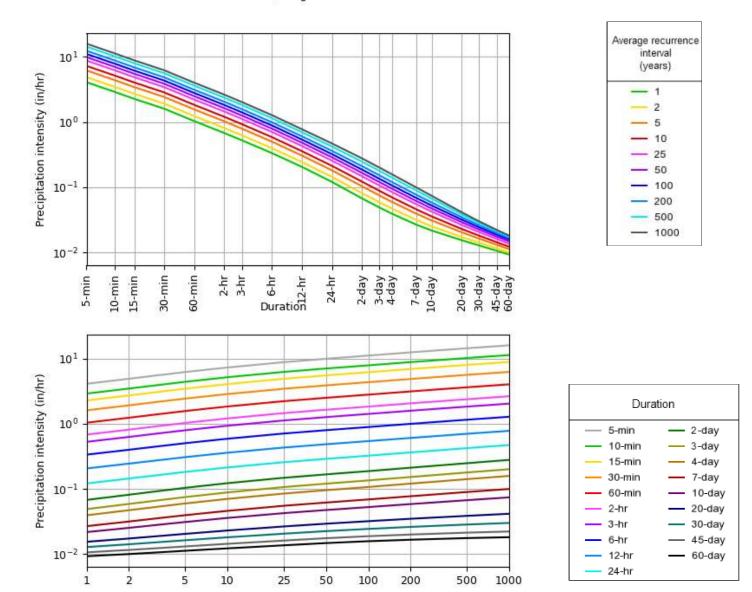
Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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#### PDS-based intensity-duration-frequency (IDF) curves Latitude: 41.4421°, Longitude: -72.0096°



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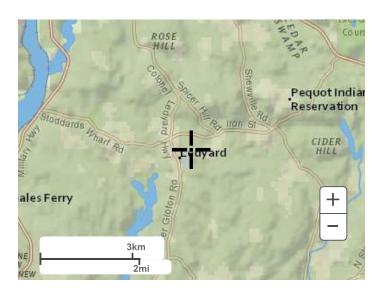
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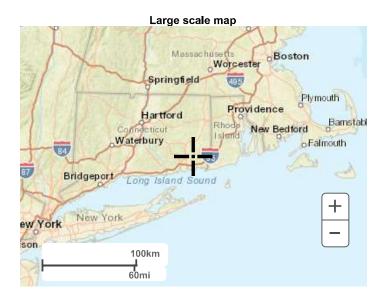
Average recurrence interval (years)

#### Maps & aerials

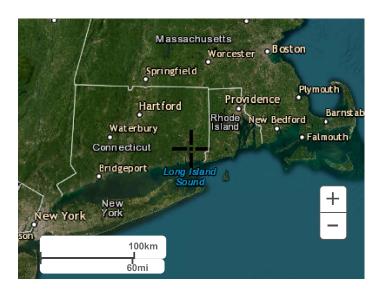
Small scale terrain







Large scale aerial



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# **APPENDIX F**

NRCS Soil Survey





Natural

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for State of Connecticut, Eastern Part



## **Preface**

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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# **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons

-

Soil Map Unit Lines

Soil Map Unit Points

#### **Special Point Features**

(9)

Blowout

 $\boxtimes$ 

Borrow Pit

**Ж** 

Clay Spot

 $\Diamond$ 

Closed Depression

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Gravel Pit

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**Gravelly Spot** 

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Landfill Lava Flow

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Marsh or swamp

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Mine or Quarry

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Miscellaneous Water

Perennial Water

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Rock Outcrop

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Saline Spot

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Sandy Spot

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Severely Eroded Spot

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Sinkhole

8

Slide or Slip

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Sodic Spot

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Spoil Area Stony Spot

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Very Stony Spot

3

Wet Spot Other

Δ.

Special Line Features

#### Water Features

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Streams and Canals

#### Transportation

Rails

~

Interstate Highways

US Routes

~

Major Roads

~

Local Roads

#### Background

10

Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12.000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: State of Connecticut, Eastern Part Survey Area Data: Version 1, Sep 15, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 14, 2022—Oct 6, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI	
3	Ridgebury, Leicester, and Whitman soils, 0 to 8 percent slopes, extremely stony	22.7	7.3%	
17	Timakwa and Natchaug soils, 0 to 2 percent slopes	1.7	0.5%	
18	Catden and Freetown soils, 0 to 2 percent slopes	1.9	0.6%	
29B	Agawam fine sandy loam, 3 to 8 percent slopes	0.3	0.1%	
45A	Woodbridge fine sandy loam, 0 to 3 percent slopes	0.1	0.0%	
45B	Woodbridge fine sandy loam, 3 to 8 percent slopes	14.5	4.6%	
46B	Woodbridge fine sandy loam, 0 to 8 percent slopes, very stony	31.3	10.0%	
47C	Woodbridge fine sandy loam, 3 to 15 percent slopes, extremely stony	40.0	12.8%	
50B	Sutton fine sandy loam, 3 to 8 percent slopes	0.1	0.0%	
51B	Sutton fine sandy loam, 0 to 8 percent slopes, very stony	34.3	11.0%	
61B	Canton and Charlton fine sandy loams, 0 to 8 percent slopes, very stony	2.9	0.9%	
61C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes, very stony	0.1	0.0%	
62C	Canton and Charlton fine sandy loams, 3 to 15 percent slopes, extremely stony	0.1	0.0%	
62D	Canton and Charlton fine sandy loams, 15 to 35 percent slopes, extremely stony	19.4	6.2%	
73C	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	49.8	15.9%	
75C	Hollis-Chatfield-Rock outcrop complex, 3 to 15 percent slopes	9.0	2.9%	
84B	Paxton and Montauk fine sandy loams, 3 to 8 percent slopes	14.1	4.5%	
85B	Paxton and Montauk fine sandy loams, 3 to 8 percent slopes, very stony	23.0	7.3%	

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
86D	Paxton and Montauk fine sandy loams, 15 to 35 percent slopes, extremely stony	14.0	4.5%
103	Rippowam fine sandy loam	11.8	3.8%
702A	Tisbury silt loam, 0 to 3 percent slopes	21.7	6.9%
Totals for Area of Interest		312.8	100.0%

### **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

#### State of Connecticut, Eastern Part

# 3—Ridgebury, Leicester, and Whitman soils, 0 to 8 percent slopes, extremely stony

#### **Map Unit Setting**

National map unit symbol: 2t2qt

Elevation: 0 to 1,480 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### Map Unit Composition

Ridgebury, extremely stony, and similar soils: 40 percent Leicester, extremely stony, and similar soils: 35 percent Whitman, extremely stony, and similar soils: 17 percent

Minor components: 8 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Ridgebury, Extremely Stony**

#### Setting

Landform: Drumlins, ground moraines, hills, drainageways, depressions

Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

#### **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 6 inches: fine sandy loam Bw - 6 to 10 inches: sandy loam

Bg - 10 to 19 inches: gravelly sandy loam Cd - 19 to 66 inches: gravelly sandy loam

#### Properties and qualities

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 15 to 35 inches to densic material

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D

Ecological site: F144AY009CT - Wet Till Depressions

Hydric soil rating: Yes

#### **Description of Leicester, Extremely Stony**

#### Setting

Landform: Ground moraines, hills, drainageways, depressions Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear

Across-slope shape: Concave

Parent material: Coarse-loamy melt-out till derived from gneiss, granite, and/or

schist

#### Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 7 inches: fine sandy loam

Bg - 7 to 18 inches: fine sandy loam

BC - 18 to 24 inches: fine sandy loam

C1 - 24 to 39 inches: gravelly fine sandy loam C2 - 39 to 65 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: High (about 9.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B/D

Ecological site: F144AY009CT - Wet Till Depressions

Hydric soil rating: Yes

#### **Description of Whitman, Extremely Stony**

#### Setting

Landform: Drumlins, ground moraines, hills, drainageways, depressions

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

#### Typical profile

Oi - 0 to 1 inches: peat

A - 1 to 10 inches: fine sandy loam

Bg - 10 to 17 inches: gravelly fine sandy loam Cdg - 17 to 61 inches: fine sandy loam

#### Properties and qualities

Slope: 0 to 3 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 7 to 38 inches to densic material

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: Frequent

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D

Ecological site: F144AY009CT - Wet Till Depressions

Hydric soil rating: Yes

#### **Minor Components**

#### Woodbridge, extremely stony

Percent of map unit: 6 percent

Landform: Hills, drumlins, ground moraines

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### **Swansea**

Percent of map unit: 2 percent Landform: Bogs, swamps Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### 17—Timakwa and Natchaug soils, 0 to 2 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2t2qx

Elevation: 0 to 1,420 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Timakwa and similar soils: 45 percent Natchaug and similar soils: 40 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Timakwa**

#### Setting

Landform: Depressions

Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Herbaceous and woody organic material over sandy and gravelly

glaciofluvial deposits

#### **Typical profile**

Oa1 - 0 to 12 inches: muck Oa2 - 12 to 37 inches: muck

2Cg1 - 37 to 47 inches: very gravelly loamy coarse sand 2Cg2 - 47 to 60 inches: gravelly loamy very fine sand

#### **Properties and qualities**

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: Rare Frequency of ponding: Frequent

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Very high (about 14.9 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D

Ecological site: F144AY042NY - Semi-Rich Organic Wetlands

Hydric soil rating: Yes

#### **Description of Natchaug**

#### Setting

Landform: Depressions, depressions, depressions Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Highly decomposed organic material over loamy glaciofluvial

deposits and/or loamy glaciolacustrine deposits and/or loamy till

#### Typical profile

Oa1 - 0 to 12 inches: muck
Oa2 - 12 to 31 inches: muck
2Cg1 - 31 to 39 inches: silt loam

2Cg2 - 39 to 79 inches: fine sandy loam

#### Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.01 to 14.17 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: Rare Frequency of ponding: Frequent

Calcium carbonate, maximum content: 25 percent Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Very high (about 17.9 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D

Ecological site: F144AY042NY - Semi-Rich Organic Wetlands

Hydric soil rating: Yes

#### **Minor Components**

#### Whitman

Percent of map unit: 7 percent

Landform: Drainageways, depressions

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Catden

Percent of map unit: 3 percent

Landform: Depressions, depressions, fens, depressions, kettles, marshes, bogs,

swamps

Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Maybid

Percent of map unit: 3 percent

Landform: Drainageways, terraces, depressions Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

#### Scarboro

Percent of map unit: 2 percent

Landform: Drainageways, outwash deltas, depressions, outwash terraces

Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Base slope, tread, dip

Down-slope shape: Concave

Across-slope shape: Linear, concave

Hydric soil rating: Yes

# 18—Catden and Freetown soils, 0 to 2 percent slopes

# **Map Unit Setting**

National map unit symbol: 2t2r2

Elevation: 0 to 1,390 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

# **Map Unit Composition**

Catden and similar soils: 45 percent Freetown and similar soils: 35 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Catden**

#### Setting

Landform: Depressions, bogs, fens, depressions, depressions, kettles, marshes,

swamps

Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Highly decomposed herbaceous organic material and/or highly

decomposed woody organic material

# **Typical profile**

Oa1 - 0 to 2 inches: muck Oa2 - 2 to 79 inches: muck

## **Properties and qualities**

Slope: 0 to 2 percent

Surface area covered with cobbles, stones or boulders: 0.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: Rare Frequency of ponding: Frequent

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Very high (about 26.9 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D

Ecological site: F144AY042NY - Semi-Rich Organic Wetlands

Hydric soil rating: Yes

## **Description of Freetown**

## Setting

Landform: Depressions, marshes, depressions, bogs, swamps, kettles

Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Highly decomposed organic material

## **Typical profile**

Oe - 0 to 2 inches: mucky peat Oa - 2 to 79 inches: muck

# Properties and qualities

Slope: 0 to 2 percent

Surface area covered with cobbles, stones or boulders: 0.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: Rare Frequency of ponding: Frequent

Available water supply, 0 to 60 inches: Very high (about 26.9 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D

Ecological site: F144AY043MA - Acidic Organic Wetlands

Hydric soil rating: Yes

#### **Minor Components**

#### **Natchaug**

Percent of map unit: 7 percent

Landform: Depressions, depressions, depressions

Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Whitman

Percent of map unit: 6 percent

Landform: Drainageways, depressions

Landform position (three-dimensional): Base slope

Down-slope shape: Concave

Across-slope shape: Concave

Hydric soil rating: Yes

#### **Timakwa**

Percent of map unit: 5 percent

Landform: Depressions

Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Scarboro

Percent of map unit: 2 percent

Landform: Depressions, drainageways, outwash deltas, outwash terraces

Landform position (three-dimensional): Base slope, tread, dip

Down-slope shape: Concave

Across-slope shape: Concave, linear

Hydric soil rating: Yes

# 29B—Agawam fine sandy loam, 3 to 8 percent slopes

## Map Unit Setting

National map unit symbol: 2tyqx

Elevation: 0 to 820 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 250 days

Farmland classification: All areas are prime farmland

# **Map Unit Composition**

Agawam and similar soils: 85 percent *Minor components:* 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Agawam**

## Setting

Landform: Outwash terraces

Landform position (three-dimensional): Tread

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Coarse-loamy eolian deposits over sandy and gravelly

glaciofluvial deposits derived from gneiss and/or granite and/or schist and/or

phyllite

# **Typical profile**

Ap - 0 to 11 inches: fine sandy loam Bw1 - 11 to 16 inches: fine sandy loam Bw2 - 16 to 26 inches: fine sandy loam 2C1 - 26 to 45 inches: loamy fine sand

2C2 - 45 to 55 inches: loamy fine sand 2C3 - 55 to 65 inches: loamy sand

# Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 15 to 35 inches to strongly contrasting textural

stratification

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.4 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: B

Ecological site: F145XY008MA - Dry Outwash

Hydric soil rating: No

## **Minor Components**

#### Merrimac

Percent of map unit: 5 percent Landform: Outwash terraces

Landform position (three-dimensional): Riser, tread

Down-slope shape: Convex Across-slope shape: Convex

Ecological site: F145XY008MA - Dry Outwash

Hydric soil rating: No

#### **Ninigret**

Percent of map unit: 4 percent

Landform: Terraces

Down-slope shape: Linear Across-slope shape: Concave

Hydric soil rating: No

#### Walpole

Percent of map unit: 3 percent

Landform: Deltas, depressions, outwash terraces, depressions, outwash plains

Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Tread, talf, dip

Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

#### Hinckley

Percent of map unit: 3 percent

Landform: Eskers

Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Ecological site: F145XY008MA - Dry Outwash

Hydric soil rating: No

# 45A—Woodbridge fine sandy loam, 0 to 3 percent slopes

## **Map Unit Setting**

National map unit symbol: 2w686

Elevation: 0 to 1,420 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

## **Map Unit Composition**

Woodbridge and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Woodbridge**

## Setting

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Footslope, summit

Landform position (three-dimensional): Crest

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

# Typical profile

Ap - 0 to 7 inches: fine sandy loam

Bw1 - 7 to 18 inches: fine sandy loam

Bw2 - 18 to 30 inches: fine sandy loam

Cd - 30 to 65 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 0 to 3 percent

Depth to restrictive feature: 20 to 39 inches to densic material

Drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 18 to 30 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.7 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C/D

Ecological site: F144AY037MA - Moist Dense Till Uplands

Hydric soil rating: No

# **Minor Components**

#### **Paxton**

Percent of map unit: 7 percent

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Summit, shoulder

Landform position (three-dimensional): Crest

Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

#### Ridgebury

Percent of map unit: 6 percent

Landform: Depressions, ground moraines, drainageways, drumlins, hills

Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Sutton

Percent of map unit: 1 percent Landform: Ground moraines, hills

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

# Whitman, extremely stony

Percent of map unit: 1 percent

Landform: Drainageways, depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# 45B—Woodbridge fine sandy loam, 3 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 2t2ql Elevation: 0 to 1,470 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Woodbridge, fine sandy loam, and similar soils: 82 percent

Minor components: 18 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Woodbridge, Fine Sandy Loam**

## Setting

Landform: Ground moraines, drumlins, hills

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

# **Typical profile**

Ap - 0 to 7 inches: fine sandy loam
Bw1 - 7 to 18 inches: fine sandy loam
Bw2 - 18 to 30 inches: fine sandy loam
Cd - 30 to 65 inches: gravelly fine sandy loam

# Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 20 to 39 inches to densic material

Drainage class: Moderately well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 18 to 30 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C/D

Ecological site: F144AY037MA - Moist Dense Till Uplands

Hydric soil rating: No

#### **Minor Components**

# Paxton

Percent of map unit: 10 percent

Landform: Drumlins, ground moraines, hills

Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Side slope, crest, nose slope

Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

## Ridgebury

Percent of map unit: 8 percent

Landform: Depressions, ground moraines, hills, drainageways

Landform position (two-dimensional): Toeslope, backslope, footslope Landform position (three-dimensional): Base slope, head slope, dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# 46B—Woodbridge fine sandy loam, 0 to 8 percent slopes, very stony

# **Map Unit Setting**

National map unit symbol: 2t2qr Elevation: 0 to 1,440 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

# **Map Unit Composition**

Woodbridge, very stony, and similar soils: 82 percent

Minor components: 18 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Woodbridge, Very Stony**

#### **Setting**

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

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# **Typical profile**

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 9 inches: fine sandy loam
Bw1 - 9 to 20 inches: fine sandy loam
Bw2 - 20 to 32 inches: fine sandy loam
Cd - 32 to 67 inches: gravelly fine sandy loam

# Properties and qualities

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Moderately well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 19 to 27 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.0 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: C/D

Ecological site: F144AY037MA - Moist Dense Till Uplands

Hydric soil rating: No

# **Minor Components**

# Paxton, very stony

Percent of map unit: 10 percent

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Shoulder, backslope, summit

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Convex, linear Across-slope shape: Linear, convex

Hydric soil rating: No

## Ridgebury, very stony

Percent of map unit: 8 percent

Landform: Depressions, ground moraines, hills, drainageways, drumlins

Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Head slope, base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# 47C—Woodbridge fine sandy loam, 3 to 15 percent slopes, extremely stony

#### Map Unit Setting

National map unit symbol: 2w685

Elevation: 10 to 1,470 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

# **Map Unit Composition**

Woodbridge, extremely stony, and similar soils: 83 percent

Minor components: 17 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Woodbridge, Extremely Stony**

#### Setting

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

# Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 9 inches: fine sandy loam
Bw1 - 9 to 20 inches: fine sandy loam
Bw2 - 20 to 32 inches: fine sandy loam
Cd - 32 to 67 inches: gravelly fine sandy loam

## Properties and qualities

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Moderately well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 19 to 27 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 5.3 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C/D

Ecological site: F144AY037MA - Moist Dense Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Paxton, extremely stony

Percent of map unit: 9 percent

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Convex, linear Across-slope shape: Linear, convex

Hydric soil rating: No

## Ridgebury, extremely stony

Percent of map unit: 5 percent

Landform: Drumlins, depressions, hills, drainageways, ground moraines

Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# Sutton, extremely stony

Percent of map unit: 2 percent Landform: Hills, ground moraines

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

# Whitman, extremely stony

Percent of map unit: 1 percent Landform: Drainageways, depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# 50B—Sutton fine sandy loam, 3 to 8 percent slopes

# **Map Unit Setting**

National map unit symbol: 2w69j

Elevation: 0 to 1,410 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

# **Map Unit Composition**

Sutton and similar soils: 80 percent *Minor components:* 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Sutton**

## Setting

Landform: Ridges, ground moraines, hills Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Coarse-loamy melt-out till derived from gneiss, granite, and/or

schist

# **Typical profile**

Ap - 0 to 5 inches: fine sandy loam
Bw1 - 5 to 17 inches: fine sandy loam
Bw2 - 17 to 25 inches: sandy loam
C1 - 25 to 39 inches: gravelly sandy loam
C2 - 39 to 60 inches: gravelly sandy loam

# Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 12 to 27 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Available water supply, 0 to 60 inches: Moderate (about 8.3 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: B/D

Ecological site: F144AY008CT - Moist Till Uplands

Hydric soil rating: No

## **Minor Components**

#### Charlton

Percent of map unit: 9 percent

Landform: Ridges, ground moraines, hills

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

#### Leicester

Percent of map unit: 5 percent

Landform: Ground moraines, hills, drainageways, depressions Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear Across-slope shape: Concave Hydric soil rating: Yes

#### Woodbridge

Percent of map unit: 5 percent

Landform: Hills, drumlins, ground moraines

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Whitman

Percent of map unit: 1 percent

Landform: Drumlins, ground moraines, hills, drainageways, depressions

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# 51B—Sutton fine sandy loam, 0 to 8 percent slopes, very stony

# **Map Unit Setting**

National map unit symbol: 2xfff Elevation: 0 to 1,410 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

## Map Unit Composition

Sutton, very stony, and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Sutton, Very Stony**

## Setting

Landform: Ground moraines, hills

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Coarse-loamy melt-out till derived from gneiss, granite, and/or

schist

## Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 7 inches: fine sandy loam
Bw1 - 7 to 19 inches: fine sandy loam
Bw2 - 19 to 27 inches: sandy loam
C1 - 27 to 41 inches: gravelly sandy loam
C2 - 41 to 62 inches: gravelly sandy loam

#### Properties and qualities

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 12 to 27 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Available water supply, 0 to 60 inches: Moderate (about 8.5 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hvdrologic Soil Group: B/D

Ecological site: F144AY008CT - Moist Till Uplands

Hydric soil rating: No

# **Minor Components**

## Charlton, very stony

Percent of map unit: 7 percent

Landform: Ridges, ground moraines, hills

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Hydric soil rating: No

# Canton, very stony

Percent of map unit: 4 percent Landform: Moraines, hills, ridges

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Hydric soil rating: No

## Leicester, very stony

Percent of map unit: 3 percent

Landform: Depressions, ground moraines, drainageways, hills Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear, concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Whitman, very stony

Percent of map unit: 1 percent

Landform: Drumlins, ground moraines, hills, drainageways, depressions

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# 61B—Canton and Charlton fine sandy loams, 0 to 8 percent slopes, very stony

# Map Unit Setting

National map unit symbol: 2w81v

Elevation: 0 to 1,480 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

# Map Unit Composition

Canton, very stony, and similar soils: 50 percent Charlton, very stony, and similar soils: 35 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Canton, Very Stony**

## Setting

Landform: Moraines, hills, ridges

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest, nose slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss,

granite, and/or schist

# **Typical profile**

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 5 inches: fine sandy loam Bw1 - 5 to 16 inches: fine sandy loam

Bw2 - 16 to 22 inches: gravelly fine sandy loam 2C - 22 to 67 inches: gravelly loamy sand

# **Properties and qualities**

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural

stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Description of Charlton, Very Stony**

#### Setting

Landform: Ridges, ground moraines, hills

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

# Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam C - 27 to 65 inches: gravelly fine sandy loam

#### Properties and qualities

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 8.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

# **Minor Components**

# Sutton, very stony

Percent of map unit: 5 percent Landform: Ground moraines, hills

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

# Leicester, very stony

Percent of map unit: 5 percent

Landform: Hills, drainageways, depressions, ground moraines Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear Across-slope shape: Concave

Hydric soil rating: Yes

#### Chatfield, very stony

Percent of map unit: 5 percent

Landform: Ridges, hills

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

# 61C—Canton and Charlton fine sandy loams, 8 to 15 percent slopes, very stony

## **Map Unit Setting**

National map unit symbol: 2w820

Elevation: 0 to 1,540 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

# **Map Unit Composition**

Canton, very stony, and similar soils: 50 percent Charlton, very stony, and similar soils: 35 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Canton, Very Stony**

#### Setting

Landform: Moraines, hills, ridges

Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Side slope, crest, nose slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss,

granite, and/or schist

#### Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 5 inches: fine sandy loam Bw1 - 5 to 16 inches: fine sandy loam

Bw2 - 16 to 22 inches: gravelly fine sandy loam 2C - 22 to 67 inches: gravelly loamy sand

# Properties and qualities

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural

stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.4 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

# **Description of Charlton, Very Stony**

## Setting

Landform: Ridges, ground moraines, hills Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

schist

# Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam C - 27 to 65 inches: gravelly fine sandy loam

## **Properties and qualities**

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 8.7 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

# **Minor Components**

# Chatfield, very stony

Percent of map unit: 5 percent

Landform: Ridges, hills

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

# Sutton, very stony

Percent of map unit: 5 percent Landform: Ground moraines, hills

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Leicester, very stony

Percent of map unit: 5 percent

Landform: Hills, drainageways, depressions, ground moraines Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear Across-slope shape: Concave Hydric soil rating: Yes

62C—Canton and Charlton fine sandy loams, 3 to 15 percent slopes,

# extremely stony

#### **Map Unit Setting**

National map unit symbol: 2wks7

Elevation: 0 to 1,310 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Canton, extremely stony, and similar soils: 50 percent Charlton, extremely stony, and similar soils: 35 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Canton, Extremely Stony**

#### Setting

Landform: Moraines, hills, ridges

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Side slope, crest, nose slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss,

granite, and/or schist

## Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 5 inches: fine sandy loam Bw1 - 5 to 16 inches: fine sandy loam

Bw2 - 16 to 22 inches: gravelly fine sandy loam 2C - 22 to 67 inches: gravelly loamy sand

# Properties and qualities

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural

stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.4 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

# **Description of Charlton, Extremely Stony**

#### **Settina**

Landform: Ridges, ground moraines, hills

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

schist

## Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam C - 27 to 65 inches: gravelly fine sandy loam

# Properties and qualities

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 8.7 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hvdrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

# **Minor Components**

## Leicester, extremely stony

Percent of map unit: 5 percent

Landform: Hills, drainageways, depressions, ground moraines Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear Across-slope shape: Concave

Hydric soil rating: Yes

# Sutton, extremely stony

Percent of map unit: 5 percent Landform: Ground moraines, hills

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

## Chatfield, extremely stony

Percent of map unit: 5 percent

Landform: Ridges, hills

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

# 62D—Canton and Charlton fine sandy loams, 15 to 35 percent slopes, extremely stony

# **Map Unit Setting**

National map unit symbol: 2w81r

Elevation: 0 to 1,640 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

# **Map Unit Composition**

Canton, extremely stony, and similar soils: 55 percent Charlton, extremely stony, and similar soils: 30 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Canton, Extremely Stony**

#### Setting

Landform: Moraines, hills, ridges

Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Side slope, nose slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss,

granite, and/or schist

## Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 5 inches: fine sandy loam Bw1 - 5 to 16 inches: fine sandy loam

Bw2 - 16 to 22 inches: gravelly fine sandy loam 2C - 22 to 67 inches: gravelly loamy sand

## **Properties and qualities**

Slope: 15 to 35 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural

stratification

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

# **Description of Charlton, Extremely Stony**

#### **Settina**

Landform: Ridges, ground moraines, hills Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

# Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam C - 27 to 65 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 15 to 35 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 8.7 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

# **Minor Components**

# Sutton, extremely stony

Percent of map unit: 5 percent Landform: Ground moraines, hills

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

# Chatfield, extremely stony

Percent of map unit: 5 percent

Landform: Ridges, hills

Landform position (two-dimensional): Summit, backslope, shoulder Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

#### Hollis, extremely stony

Percent of map unit: 5 percent

Landform: Ridges, hills

Landform position (two-dimensional): Shoulder, backslope, summit Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

# 73C—Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky

# Map Unit Setting

National map unit symbol: 2w698

Elevation: 0 to 1,550 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Charlton, very stony, and similar soils: 50 percent Chatfield, very stony, and similar soils: 30 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Charlton, Very Stony**

## Setting

Landform: Ridges, hills

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Side slope, crest, nose slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

schist

# **Typical profile**

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam C - 27 to 65 inches: gravelly fine sandy loam

# Properties and qualities

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 8.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

# **Description of Chatfield, Very Stony**

## Setting

Landform: Hills, ridges

Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

schist

# **Typical profile**

Oi - 0 to 1 inches: slightly decomposed plant material

A - 1 to 2 inches: fine sandy loam

Bw - 2 to 30 inches: gravelly fine sandy loam

2R - 30 to 40 inches: bedrock

## **Properties and qualities**

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 20 to 41 inches to lithic bedrock

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.3 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

# **Minor Components**

## Sutton, very stony

Percent of map unit: 5 percent Landform: Ground moraines, hills

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### **Rock outcrop**

Percent of map unit: 5 percent

Hydric soil rating: No

# Hollis, very stony

Percent of map unit: 5 percent

Landform: Hills, ridges

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

# Leicester, very stony

Percent of map unit: 5 percent

Landform: Drainageways, depressions

Down-slope shape: Linear Across-slope shape: Concave

Hydric soil rating: Yes

# 75C—Hollis-Chatfield-Rock outcrop complex, 3 to 15 percent slopes

#### Map Unit Setting

National map unit symbol: 9lqn Elevation: 0 to 1.200 feet

Mean annual precipitation: 43 to 56 inches
Mean annual air temperature: 45 to 55 degrees F

Frost-free period: 140 to 185 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Hollis and similar soils: 35 percent Chatfield and similar soils: 30 percent

Rock outcrop: 15 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Hollis**

#### Settina

Landform: Ridges, hills Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy melt-out till derived from granite and/or schist and/or

gneiss

# **Typical profile**

Oa - 0 to 1 inches: highly decomposed plant material

A - 1 to 6 inches: gravelly fine sandy loam

Bw1 - 6 to 9 inches: channery fine sandy loam Bw2 - 9 to 15 inches: gravelly fine sandy loam

2R - 15 to 80 inches: bedrock

## Properties and qualities

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Somewhat excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Low to high (0.01 to

5.95 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 1.8 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

## **Description of Chatfield**

## Setting

Landform: Ridges, hills Down-slope shape: Convex Across-slope shape: Linear

Parent material: Coarse-loamy melt-out till derived from granite and/or schist

and/or gneiss

# **Typical profile**

Oa - 0 to 1 inches: highly decomposed plant material

A - 1 to 6 inches: gravelly fine sandy loam
Bw1 - 6 to 15 inches: gravelly fine sandy loam
Bw2 - 15 to 29 inches: gravelly fine sandy loam
2R - 29 to 80 inches: unweathered bedrock

# **Properties and qualities**

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Low to high (0.01 to

5.95 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

## **Description of Rock Outcrop**

# **Typical profile**

R - 0 to 0 inches: bedrock

#### **Properties and qualities**

Slope: 3 to 15 percent

Depth to restrictive feature: 0 inches to lithic bedrock

Runoff class: Very high

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydrologic Soil Group: D Hydric soil rating: Unranked

#### **Minor Components**

#### Charlton

Percent of map unit: 7 percent

Landform: Hills

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

#### Sutton, very stony

Percent of map unit: 5 percent

Landform: Drainageways, depressions

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Leicester

Percent of map unit: 5 percent

Landform: Drainageways, depressions

Down-slope shape: Linear Across-slope shape: Concave

Hydric soil rating: Yes

#### **Brimfield**

Percent of map unit: 1 percent

Landform: Ridges, hills Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

# Unnamed, red parent material

Percent of map unit: 1 percent

Hydric soil rating: No

#### Unnamed, sandy subsoil

Percent of map unit: 1 percent

Hydric soil rating: No

# 84B—Paxton and Montauk fine sandy loams, 3 to 8 percent slopes

## **Map Unit Setting**

National map unit symbol: 2t2qn Elevation: 0 to 1,570 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

## **Map Unit Composition**

Paxton and similar soils: 55 percent Montauk and similar soils: 30 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Paxton**

## Setting

Landform: Ground moraines, drumlins, hills

Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Nose slope, side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or schist

#### Typical profile

Ap - 0 to 8 inches: fine sandy loam
Bw1 - 8 to 15 inches: fine sandy loam
Bw2 - 15 to 26 inches: fine sandy loam
Cd - 26 to 65 inches: gravelly fine sandy loam

# **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: 18 to 39 inches to densic material

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.1 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

# **Description of Montauk**

#### Setting

Landform: Hills, drumlins Down-slope shape: Convex Across-slope shape: Linear

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

#### Typical profile

A - 0 to 4 inches: fine sandy loam
Bw1 - 4 to 14 inches: fine sandy loam
Bw2 - 14 to 25 inches: sandy loam

2Cd1 - 25 to 39 inches: gravelly loamy coarse sand 2Cd2 - 39 to 60 inches: gravelly sandy loam

# Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 20 to 38 inches to densic material

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: About 24 to 30 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Woodbridge

Percent of map unit: 5 percent

Landform: Drumlins, hills, ground moraines

Landform position (two-dimensional): Footslope, backslope, summit

Landform position (three-dimensional): Side slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Ridgebury

Percent of map unit: 5 percent

Landform: Depressions, ground moraines, hills, drainageways Landform position (two-dimensional): Toeslope, backslope, footslope

Landform position (three-dimensional): Base slope, head slope, dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# Charlton

Percent of map unit: 5 percent

Landform: Hills

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

# 85B—Paxton and Montauk fine sandy loams, 3 to 8 percent slopes, very stony

# **Map Unit Setting**

National map unit symbol: 2w679

Elevation: 0 to 1,530 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Paxton, very stony, and similar soils: 55 percent Montauk, very stony, and similar soils: 30 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Paxton, Very Stony**

#### Setting

Landform: Hills, ground moraines, drumlins

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

#### Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 10 inches: fine sandy loam

Bw1 - 10 to 17 inches: fine sandy loam

Bw2 - 17 to 28 inches: fine sandy loam

Cd - 28 to 67 inches: gravelly fine sandy loam

#### Properties and qualities

Slope: 3 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.8 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

## **Description of Montauk, Very Stony**

## Setting

Landform: Recessionial moraines, ground moraines, hills, drumlins Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy lodgment till derived from gneiss,

granite, and/or schist

#### **Typical profile**

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 6 inches: fine sandy loam
Bw1 - 6 to 28 inches: fine sandy loam
Bw2 - 28 to 36 inches: sandy loam

2Cd - 36 to 74 inches: gravelly loamy sand

# **Properties and qualities**

Slope: 3 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 1.42 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 5.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

## **Minor Components**

## Woodbridge, very stony

Percent of map unit: 8 percent

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

## Charlton, very stony

Percent of map unit: 3 percent

Landform: Hills

Landform position (two-dimensional): Shoulder, summit, backslope

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

## Ridgebury, very stony

Percent of map unit: 3 percent

Landform: Drumlins, depressions, ground moraines, hills, drainageways

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

# Stockbridge, very stony

Percent of map unit: 1 percent

Landform: Hills

Landform position (two-dimensional): Shoulder, backslope, summit

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

# 86D—Paxton and Montauk fine sandy loams, 15 to 35 percent slopes, extremely stony

# **Map Unit Setting**

National map unit symbol: 2w67c

Elevation: 0 to 1,400 feet

Mean annual precipitation: 36 to 71 inches

Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Paxton, extremely stony, and similar soils: 55 percent Montauk, extremely stony, and similar soils: 30 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Paxton, Extremely Stony**

## Setting

Landform: Ground moraines, hills, drumlins
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Side slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

# **Typical profile**

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 10 inches: fine sandy loam

Bw1 - 10 to 17 inches: fine sandy loam

Bw2 - 17 to 28 inches: fine sandy loam

Cd - 28 to 67 inches: gravelly fine sandy loam

## **Properties and qualities**

Slope: 15 to 35 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.8 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hvdrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

# **Description of Montauk, Extremely Stony**

# Setting

Landform: Hills, recessionial moraines, ground moraines, drumlins

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy lodgment till derived from gneiss,

granite, and/or schist

## Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 6 inches: fine sandy loam
Bw1 - 6 to 28 inches: fine sandy loam
Bw2 - 28 to 36 inches: sandy loam

2Cd - 36 to 74 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 15 to 35 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 1.42 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 5.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

# **Minor Components**

# Charlton, extremely stony

Percent of map unit: 6 percent

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

# Woodbridge, extremely stony

Percent of map unit: 5 percent

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

# Ridgebury, extremely stony

Percent of map unit: 3 percent

Landform: Drumlins, depressions, ground moraines, hills, drainageways

Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

## Stockbridge, extremely stony

Percent of map unit: 1 percent

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

# 103—Rippowam fine sandy loam

# **Map Unit Setting**

National map unit symbol: 9ljp Elevation: 0 to 1,200 feet

Mean annual precipitation: 43 to 54 inches Mean annual air temperature: 45 to 55 degrees F

Frost-free period: 140 to 185 days

Farmland classification: Farmland of statewide importance

## **Map Unit Composition**

Rippowam and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Rippowam**

## Setting

Landform: Flood plains
Down-slope shape: Linear
Across-slope shape: Concave

Parent material: Coarse-loamy alluvium

# **Typical profile**

A - 0 to 5 inches: fine sandy loam
Bg1 - 5 to 12 inches: fine sandy loam
Cg2 - 12 to 19 inches: fine sandy loam
Cg3 - 19 to 24 inches: sandy loam
Cg4 - 24 to 27 inches: sandy loam
Cg5 - 27 to 31 inches: loamy sand

Cg6 - 31 to 65 inches: stratified very gravelly coarse sand to loamy fine sand

## **Properties and qualities**

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 5.95 in/hr)

Depth to water table: About 0 to 18 inches

Frequency of flooding: Frequent Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 5.9 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: B/D

Ecological site: F144AY014CT - Wet Sandy Low Floodplain

Hydric soil rating: Yes

## **Minor Components**

## Occum

Percent of map unit: 5 percent Landform: Flood plains Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

### Suncook

Percent of map unit: 5 percent Landform: Flood plains Down-slope shape: Linear Across-slope shape: Convex Hydric soil rating: No

### Lim

Percent of map unit: 3 percent Landform: Flood plains Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

## **Pootatuck**

Percent of map unit: 3 percent Landform: Flood plains Down-slope shape: Linear Across-slope shape: Concave Hydric soil rating: No

## Limerick

Percent of map unit: 2 percent Landform: Flood plains Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

## Saco

Percent of map unit: 2 percent Landform: Flood plains Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

## 702A—Tisbury silt loam, 0 to 3 percent slopes

## **Map Unit Setting**

National map unit symbol: 2y07g

Elevation: 0 to 1,260 feet

Mean annual precipitation: 43 to 54 inches Mean annual air temperature: 45 to 55 degrees F

Frost-free period: 140 to 185 days

Farmland classification: All areas are prime farmland

## **Map Unit Composition**

Tisbury and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Tisbury**

## Setting

Landform: Outwash terraces, deltas, outwash plains, valley trains

Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Coarse-silty eolian deposits over sandy and gravelly glaciofluvial

deposits derived from granite, schist, and/or gneiss

## Typical profile

Ap - 0 to 8 inches: silt loam
Bw1 - 8 to 18 inches: silt loam
Bw2 - 18 to 26 inches: silt loam

2C - 26 to 65 inches: extremely gravelly sand

## Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: 24 to 36 inches to strongly contrasting textural

stratification

Drainage class: Moderately well drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 16 to 30 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.3 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B/D

Ecological site: F144AY026CT - Moist Silty Outwash

Hydric soil rating: No

## **Minor Components**

### Merrimac

Percent of map unit: 5 percent

Landform: Outwash plains, outwash terraces, moraines, eskers, kames

Landform position (two-dimensional): Shoulder, summit

Landform position (three-dimensional): Side slope, crest, tread

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

## Agawam

Percent of map unit: 5 percent

Landform: Kame terraces, outwash plains, outwash terraces, moraines, kames

Landform position (two-dimensional): Summit, shoulder

Landform position (three-dimensional): Side slope, crest, tread

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

## **Ninigret**

Percent of map unit: 3 percent

Landform: Kames, outwash terraces, kame terraces, outwash plains, moraines

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Convex, linear Across-slope shape: Convex, concave

Hydric soil rating: No

## Raypol

Percent of map unit: 2 percent

Landform: Drainageways, depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# Soil Information for All Uses

## **Soil Properties and Qualities**

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

## Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

## **Hydrologic Soil Group**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

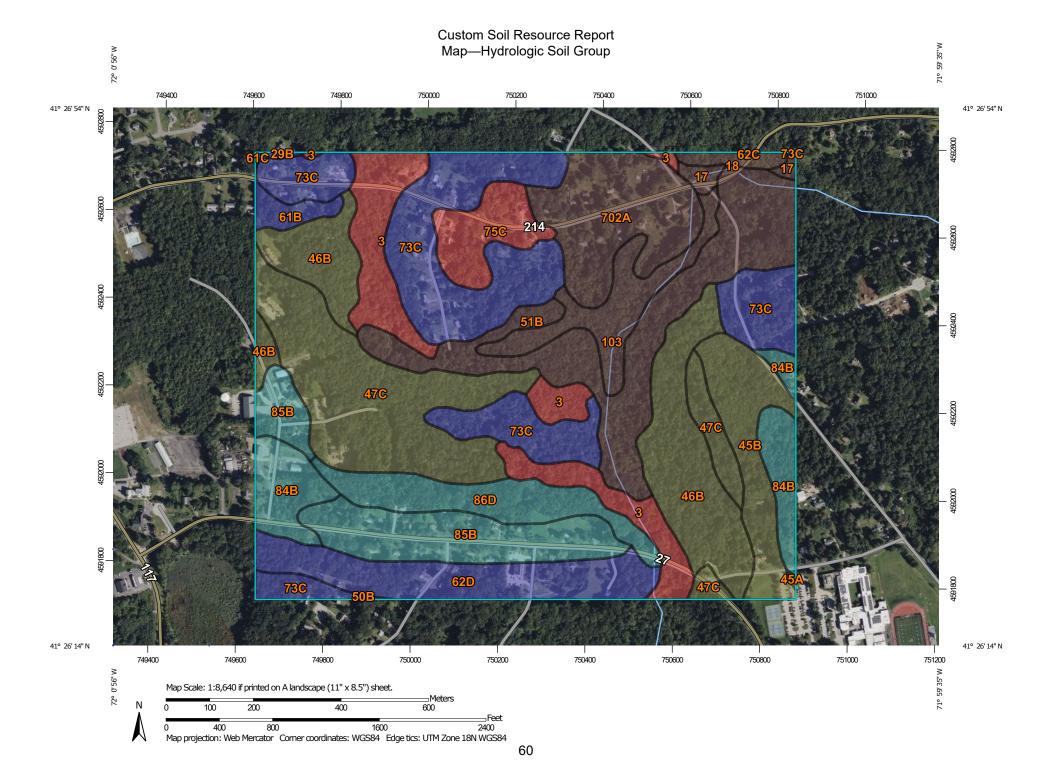
Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.



#### MAP LEGEND MAP INFORMATION Area of Interest (AOI) The soil surveys that comprise your AOI were mapped at С 1:12.000. Area of Interest (AOI) C/D Soils Please rely on the bar scale on each map sheet for map D Soil Rating Polygons measurements. Not rated or not available Α Source of Map: Natural Resources Conservation Service **Water Features** A/D Web Soil Survey URL: Streams and Canals В Coordinate System: Web Mercator (EPSG:3857) Transportation B/D Rails ---Maps from the Web Soil Survey are based on the Web Mercator С projection, which preserves direction and shape but distorts Interstate Highways distance and area. A projection that preserves area, such as the C/D **US Routes** Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. D Major Roads ~ Not rated or not available -Local Roads This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Rating Lines Background Aerial Photography Soil Survey Area: State of Connecticut, Eastern Part Survey Area Data: Version 1, Sep 15, 2023 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Jun 14, 2022—Oct 6, C/D 2022 The orthophoto or other base map on which the soil lines were Not rated or not available compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor **Soil Rating Points** shifting of map unit boundaries may be evident. Α A/D B/D

## Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
3	Ridgebury, Leicester, and Whitman soils, 0 to 8 percent slopes, extremely stony	D	22.7	7.3%
17	Timakwa and Natchaug soils, 0 to 2 percent slopes	B/D	1.7	0.5%
18	Catden and Freetown soils, 0 to 2 percent slopes	B/D	1.9	0.6%
29B	Agawam fine sandy loam, 3 to 8 percent slopes	В	0.3	0.1%
45A	Woodbridge fine sandy loam, 0 to 3 percent slopes	C/D	0.1	0.0%
45B	Woodbridge fine sandy loam, 3 to 8 percent slopes	C/D	14.5	4.6%
46B	Woodbridge fine sandy loam, 0 to 8 percent slopes, very stony	C/D	31.3	10.0%
47C	Woodbridge fine sandy loam, 3 to 15 percent slopes, extremely stony	C/D	40.0	12.8%
50B	Sutton fine sandy loam, 3 to 8 percent slopes	B/D	0.1	0.0%
51B	Sutton fine sandy loam, 0 to 8 percent slopes, very stony	B/D	34.3	11.0%
61B	Canton and Charlton fine sandy loams, 0 to 8 percent slopes, very stony	В	2.9	0.9%
61C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes, very stony	В	0.1	0.0%
62C	Canton and Charlton fine sandy loams, 3 to 15 percent slopes, extremely stony	В	0.1	0.0%
62D	Canton and Charlton fine sandy loams, 15 to 35 percent slopes, extremely stony	В	19.4	6.2%
73C	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	В	49.8	15.9%

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
75C	Hollis-Chatfield-Rock outcrop complex, 3 to 15 percent slopes	D	9.0	2.9%
84B	Paxton and Montauk fine sandy loams, 3 to 8 percent slopes	С	14.1	4.5%
85B	Paxton and Montauk fine sandy loams, 3 to 8 percent slopes, very stony	С	23.0	7.3%
86D	Paxton and Montauk fine sandy loams, 15 to 35 percent slopes, extremely stony	С	14.0	4.5%
103	Rippowam fine sandy loam	B/D	11.8	3.8%
702A	Tisbury silt loam, 0 to 3 percent slopes	B/D	21.7	6.9%
Totals for Area of Inter	est		312.8	100.0%

## Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified

Tie-break Rule: Higher

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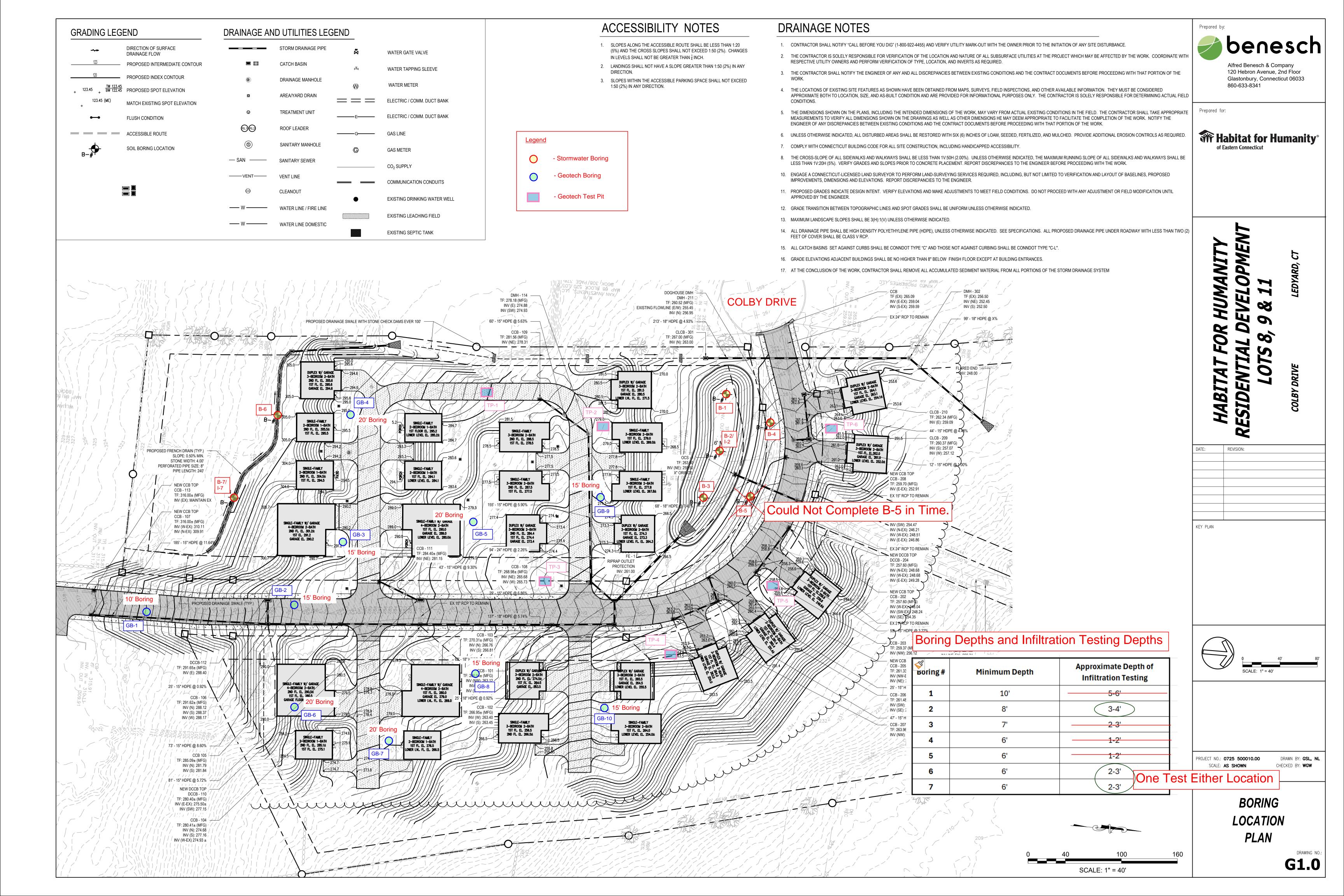
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# **APPENDIX G**

Test Pits & Infiltration Results







# Test Boring Falling Head Test Proposed Habitat for Humanity Development Colby Drive Ledyard, CT File No. 0015-046.00

Test Location:I-2Driller:J. CassonTest Type:Falling HeadEngineer:M. FekietaDate:11/5/2024Weather:Sunny, 60s

Ground surface El.: 262.0 (ft.) Total Casing Length: 5.5 (ft.) Inside Casing Diameter: 4 (in.)

Top of Casing El.: 264.5 (ft.)
Bottom of Casing El.: 259.0 (ft.)

## Hydraulic Conductivity (Kv) = $\pi$ [D {Ln (h1/h2)}] / 11 (t2-t1)

Elapsed Time	t2 - t1	DTW	h1	h2	In(h1/h2)	Kv	Kv	Kv
(min.)	(min.)	(in.)	(in.)	(in.)	111(111/112)	(in/min)	(cm/sec)	(in/hr)
4.0	4.0	0.5	66.5	66.0	0.0075	2.2E-03	9.1E-05	1.3E-01
8	4.0	1.3	66.0	65.3	0.0114	3.3E-03	1.4E-04	2.0E-01
12	4.0	2.0	65.3	64.5	0.0116	3.3E-03	1.4E-04	2.0E-01
24	12.0	4.0	64.5	62.5	0.0315	3.0E-03	1.3E-04	1.8E-01
36	12.0	6.0	62.5	60.5	0.0325	3.1E-03	1.3E-04	1.9E-01
58	22.0	10.0	60.5	56.5	0.0684	3.6E-03	1.5E-04	2.1E-01
100	42.0	17.0	56.5	49.5	0.1323	3.6E-03	1.5E-04	2.2E-01
144	44.0	23.0	49.5	43.5	0.1292	3.4E-03	1.4E-04	2.0E-01
171	27.0	27.3	43.5	39.3	0.1028	4.3E-03	1.8E-04	2.6E-01
214	43.0	33.0	39.3	33.5	0.1584	4.2E-03	1.8E-04	2.5E-01
245	31.0	36.5	33.5	30.0	0.1103	4.1E-03	1.7E-04	2.4E-01

Average 3.4E-03 1.5E-04 2.1E-01



# Test Boring Falling Head Test Proposed Habitat for Humanity Development Colby Drive Ledyard, CT File No. 0015-046.00

Test Location:I-7Driller:Jim CassonTest Type:Falling HeadEngineer:M. FekietaDate:11/5/2024Weather:Sunny 60s

Ground surface El.: 311.0 (ft.) Total Casing Length: 5.5 (ft.) Inside Casing Diameter: 4 (in.)

Top of Casing El.: 313.4 (ft.)
Bottom of Casing El.: 307.9 (ft.)

## Hydraulic Conductivity (Kv) = $\pi$ [D {Ln (h1/h2)}] / 11 (t2-t1)

Elapsed Time	t2 - t1	DTW	h1	h2	ln(h1/h2)	Kv	Kv	Kv
(min.)	(min.)	(in.)	(in.)	(in.)	111(111/112)	(in/min)	(cm/sec)	(in/hr)
1.0	1.0	0.5	66.0	65.5	0.0076	8.7E-03	3.7E-04	5.2E-01
2	1.0	1.3	65.5	64.8	0.0115	1.3E-02	5.6E-04	7.9E-01
4	2.0	3.0	64.8	63.0	0.0274	1.6E-02	6.6E-04	9.4E-01
6	2.0	4.5	63.0	61.5	0.0241	1.4E-02	5.8E-04	8.3E-01
10	4.0	7.5	61.5	58.5	0.0500	1.4E-02	6.0E-04	8.6E-01
16	6.0	11.8	58.5	54.3	0.0754	1.4E-02	6.1E-04	8.6E-01
32	16.0	21.8	54.3	44.3	0.2037	1.5E-02	6.2E-04	8.7E-01
45	13.0	29.5	44.3	36.5	0.1925	1.7E-02	7.2E-04	1.0E+00
70	25.0	40.8	36.5	25.3	0.3685	1.7E-02	7.1E-04	1.0E+00
89	19.0	48.0	25.3	18.0	0.3385	2.0E-02	8.6E-04	1.2E+00
105	16.0	53.0	18.0	13.0	0.3254	2.3E-02	9.8E-04	1.4E+00

Average	1.6E-02	6.6E-04	9.4E-01



## PROPOSED HABITAT FOR HUMANITY DEVELOPMENT

COLBY DRIVE

LEDYARD, CONNECTICUT

BORING NO. B-1

SHEET 1 of 1

FILE NO. 0015-046.00

CHKD. BY TJO

Boring Co.	General Borings, Inc.	Boring Location	5	See Boring Loca	ation Plan
Driller	Jim Casson	Ground Surface El.	264.5'+/-	Datum	Not Available
Logged By _	Mateusz Fekieta	Date Start	10/24/2024	Date End	11/5/2024

Hammer Type:	Automatic Hammer		Ground	water Reading	js (from	ground surface)
Sampler Size:	1-3/8" I.D. Split Spoon	Date	Time	Depth (ft)	Elev.	Stabilization Time
Type Drill Rig:	Truck Mounted Diedrich D-50	11/5/24	-	7	-	Moist Sample
Drilling Method:	3.25-inch I.D. Hollow-Stem Augers	11/5/24	-	10.5	254'+/-	End of Boring

SAMPLE INFORMATION   SAMPLE DESCRIPTION   STRATA	D E	Metrioc	u.	e A I	5.25-IIIGH I.D. HOHOW-STEHLAU					
1	P Ca								SIRAIA	
Subscript										
S-2   18/24   2 to 4   7-17-28-38   Dense, brown, fine to coarse SAND, some Silt, little fine to coarse Gravel	1		S-1	15/24	0 to 2	1-2-4-4			6"+/- Topsoil	
								trace (-) Roots	SUBSOIL	
Signature   Sign		L	S-2	18/24	2 to 4	7-17-28-38		Dense, brown, fine to coarse SAND, some Silt, little fine to coarse Gravel		
S-3   20/24   5 to 7   14-32-17-20   Dense, brown, fine to coarse SAND, some Silt, little fine to coarse Gravel   TILL									-	
Till	_	-	S-3	20/24	5 to 7	14-32-17-20			1	
8   S-4   20/24   7 to 9   29-14-19-25   Dense, brown, fine to coarse SAND, little fline to coarse Gravel, moist	_		-	20/21	0.01	02 20		Dense, brown, fine to coarse SAND, some Silt, little fine to coarse Gravel	TILL	
9   0   0   5   18/18   9 to 10.5   17-29-50/6"   Very dense, gray, fine to coarse SAND, some Silt, little fine to coarse Gravel	_		S-4	20/24	7 to 9	29-14-19-25		Dance brown fine to coarse SAND little Silt little fine to coarse Cravel maint	1	
11								Derise, drown, line to coarse SAND, little Silt, little line to coarse Graver, moist		
END OF EXPLORATION AT 10.5 FEET BELOW GROUND SURFACE  END OF EXPLORATION AT 10.5 FEET BELOW GROUND SUR			S-5	18/18	9 to 10.5	17-29-50/6"		Very dense, gray, fine to coarse SAND, some Silt, little fine to coarse Gravel		
13	_	-								
144								END OF EXPLORATION AT 10.5 FEET BELOW GROUND SURFACE		
15	_	-								
16										
17	_	-								
18										
20	_	Ī								
21	19									
22										
23	_	_								
24										
25	_	-								
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34	-	_								
35		}								
36	-	$\dashv$	-							
37		}								
38		$\dashv$								
39										
40										

SPT N-Values	SPT N-Values	Proportions	SYMBO	L KEY
0 to 4 - Very Loose	0 to 2 - Very Soft	Trace = 0 to 10%	S denotes split-barrel sampler.	7. WH denotes weight of hammer
5 to 10 - Loose	3 to 4 - Soft	Little = 10 to 20%	ST denotes 3-inch O.D. undisturbed sample.	8. WR denotes weight of rods
11 to 30 - Medium Dense	5 to 8 - Medium Stiff	Some = 20 to 35%	3. UO denotes 3-inch Osterberg undisturbed sample.	PP denotes Pocket Penetrometer.
31 to 50 - Dense	9 to 15 - Stiff	And = 35 to 50%	PEN denotes penetration length of sampler.	10. FVST denotes field vane shear test.
Over 50 - Very Dense	16 to 30 - Very Stiff		<ol><li>REC denotes recovered length of sample.</li></ol>	11. RQD denotes Rock Quality Designation.
	Over 30 - Hard		SPT denotes Standard Penetration Test.	12. C denotes core run number.

<sup>2)</sup> Water level readings have been made at times and under conditions stated, fluctuations may occur due to other factors.

<sup>3)</sup> Cobbles and/or boulders were inferred based on observed auger chatter from about 4.5 to 5.5 and 8.5 to 9.5 feet below grade.



## PROPOSED HABITAT FOR HUMANITY DEVELOPMENT

COLBY DRIVE

LEDYARD, CONNECTICUT

BORING NO. B-2

SHEET 1 of 1

FILE NO. 0015-046.00

TJO

CHKD. BY

Boring Co.	General Borings, Inc.	Boring Location	5	ation Plan	
Oriller	Jim Casson	Ground Surface El.	262'+/-	Datum	Not Available
ogged By	Mateusz Fekieta	Date Start	10/24/2024	Date End	10/24/2024

Hammer Type:	Automatic Hammer	Groundwater Readings (from ground surface)				ground surface)
Sampler Size:	1-3/8" I.D. Split Spoon	Date	Time	Depth (ft)	Elev.	Stabilization Time
Type Drill Rig:	Truck Mounted Diedrich D-50	10/24/24	-	5	257'+/-	Perched Water
Drilling Method:	3.25-inch I.D. Hollow-Stem Augers					

Drillin	ng Metho	oa:			3.25-inch I.D. Hollo	w-Stem Au	gers	
E P	Casing		SAI	MPLE INFO	RMATION		SAMPLE DESCRIPTION	STRATA
T H	Blows (ft)	Type & No.	REC/PEN (inches)	DEPTH (feet)	BLOWS PER 6 INCHES	Core Time (min./ft)		
1	, ,		, ,	,,				8"+/- Topsoil
2		S-1	0/12	1 to 2	7-10-50/0"		Very dense, No Recovery	SUBSOIL
3		S-2	24/24	2 to 4	4-14-20-18		· · ·	
4							Dense, brown to gray-brown, fine to coarse SAND, some Silt, little fine to coarse Gravel	
5		S-3	16/24	4 to 6	8-30-46-50		Very dense, Top 6": orange-brown, fine SAND, some Silt, wet;	
6							Bottom 10": gray-brown, fine to coarse SAND, some Silt, little fine to coarse Gravel, dry	TILL
7		S-4	18/24	6 to 8	20-15-22-29		Dense, gray, fine to coarse SAND, some Silt, little fine to coarse Gravel, moist	
8								
9							END OF EXPLORATION AT 8 FEET BELOW GROUND SURFACE	
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	CDT	AL Mali	/alues SPT N-Values Pr			I Drai	portions SYMBOL KEY	

SPT N-Values	SPT N-Values	Proportions	SYMBO	L KEY				
0 to 4 - Very Loose	0 to 4 - Very Loose 0 to 2 - Very Soft		S denotes split-barrel sampler.	7. WH denotes weight of hammer				
5 to 10 - Loose 3 to 4 - Soft		Little = 10 to 20%	ST denotes 3-inch O.D. undisturbed sample.	8. WR denotes weight of rods				
11 to 30 - Medium Dense	5 to 8 - Medium Stiff	Some = 20 to 35%	3. UO denotes 3-inch Osterberg undisturbed sample.	PP denotes Pocket Penetrometer.				
31 to 50 - Dense	31 to 50 - Dense 9 to 15 - Stiff		4. PEN denotes penetration length of sampler.	10. FVST denotes field vane shear test.				
Over 50 - Very Dense	16 to 30 - Very Stiff		<ol><li>REC denotes recovered length of sample.</li></ol>	11. RQD denotes Rock Quality Designation.				
	Over 30 - Hard		SPT denotes Standard Penetration Test.	12. C denotes core run number.				

- 2) Water level readings have been made at times and under conditions stated, fluctuations may occur due to other factors.
- 3) Cobbles and/or boulders were inferred based on observed auger chatter from about 0 to 4 feet below grade.



## PROPOSED HABITAT FOR HUMANITY DEVELOPMENT

COLBY DRIVE

LEDYARD, CONNECTICUT

BORING NO. \_\_\_\_

B-3 1 of 1

FILE NO. 0015-046.00 CHKD. BY TJO

Boring Co.	General Borings, Inc.	Boring Location	S	ation Plan	
Oriller	Jim Casson	Ground Surface El.	261'+/-	Datum	Not Available
ogged By	Mateusz Fekieta	Date Start	11/5/2024	Date End	11/5/2024

Hammer Type:	Automatic Hammer	Groundwater Readings (from ground surface)				ground surface)
Sampler Size:	1-3/8" I.D. Split Spoon	Date	Time	Depth (ft)	Elev.	Stabilization Time
Type Drill Rig:	Truck Mounted Diedrich D-50	11/5/24	-	-	-	Not Encountered
Drilling Method:	3.25-inch LD. Hollow-Stem Augers					

D E P	Casing						SAMPLE DESCRIPTION	STRATA	
T H	Blows (ft)	Type & No.	REC/PEN (inches)	DEPTH (feet)	BLOWS PER 6 INCHES	Core Time (min./ft)			
1									9"+/- Topsoil
2		S-1	10/24	1 to 3	2-6-13-21			Medium dense, orange-brown, fine SAND, some Silt	SUBSOIL
3								Medium dense, drange-brown, line OAND, some Silt	
4		S-2	2/19	3 to 4.7	22-20-33-50/1"			Very dense, gray, fractured COBBLE fragments	
5								, , , , , , , , , , , , , , , , , , , ,	TILL
6		S-3	19/24	5 to 7	19-21-18-16		Dei	nse, gray, fine to coarse SAND, some Silt, little fine to coarse Gravel	
7 8								ND OF EXPLORATION AT 7 FEET BELOW GROUND SURFACE	
9							_	IND OF EXPLORATION AT 7 FEET BELOW GROUND SURFACE	
10									
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	SPT	N-Valu	ies	SP1	Γ N-Values	Prop	ortions	SYMBOL KEY	

_								
	SPT N-Values	SPT N-Values	Proportions	SYMBOL KEY				
Г	0 to 4 - Very Loose	0 to 2 - Very Soft	Trace = 0 to 10%	S denotes split-barrel sampler.	7. WH denotes weight of hammer			
1	5 to 10 - Loose 3 to 4 - Soft		Little = 10 to 20%	2. ST denotes 3-inch O.D. undisturbed sample.	8. WR denotes weight of rods			
1	11 to 30 - Medium Dense	5 to 8 - Medium Stiff	Some = 20 to 35%	3. UO denotes 3-inch Osterberg undisturbed sample.	PP denotes Pocket Penetrometer.			
1	31 to 50 - Dense 9 to 15 - Stiff		And = 35 to 50%	4. PEN denotes penetration length of sampler.	10. FVST denotes field vane shear test.			
1	Over 50 - Very Dense	16 to 30 - Very Stiff		5. REC denotes recovered length of sample.	11. RQD denotes Rock Quality Designation.			
1		Over 30 - Hard		SPT denotes Standard Penetration Test.	12. C denotes core run number.			

<sup>2)</sup> Water level readings have been made at times and under conditions stated, fluctuations may occur due to other factors.

<sup>3)</sup> Cobbles and/or boulders were inferred based on observed auger chatter from about 3 to 5 feet below grade.



## PROPOSED HABITAT FOR HUMANITY DEVELOPMENT

COLBY DRIVE

LEDYARD, CONNECTICUT

 BORING NO.
 B-4

 SHEET
 1 of 1

 FILE NO.
 0015-046.00

 CHKD. BY
 TJO

Boring Co.	General Borings, Inc.	Boring Location		ition Plan	
Oriller	Jim Casson	Ground Surface El.	261'+/-	Datum	Not Available
_ogged By _	Mateusz Fekieta	Date Start	11/5/2024	Date End	11/5/2024

Hammer Type:	Automatic Hammer	Groundwater Readings (from ground surface)				ground surface)
Sampler Size:	1-3/8" I.D. Split Spoon	Date	Time	Depth (ft)	Elev.	Stabilization Time
Type Drill Rig:	Truck Mounted Diedrich D-50	11/5/24	-	-	-	Not Encountered
Drilling Method:	3.25-inch I.D. Hollow-Stem Augers					

	rilling Method:			3.25-inch I.D. Hollow-Stem Augers			gers						
D E			SAI	MPLE INFO	RMATION				SAMPL	E DESCRIPT	ION		STRATA
Р	Casing												
T H	Blows (ft)	Type & No.	REC/PEN (inches)	DEPTH (feet)	BLOWS PER 6 INCHES	Core Time (min./ft)							
1		S-1	20/24	0 to 2	2-6-5-5			Mar all	d	6	CAND	0:14	9"+/- Topsoil
2								Medium	dense, orang	ge-brown, fine	SAND, son	ne Silt	SUBSOIL
3		S-2	20/24	2 to 4	7-13-19-43		Dense	brown to grav	fine to coars	SE SAND little	fine to coal	se Gravel, little Silt	
4													TILL
5		S-3	10/15	4 to 5.3	43-39-50/3"							to coarse Gravel	
6							EN	D OF EXPLO	RATION AT	5.3 FEET BEL	LOW GROU	ND SURFACE	
7 8													
9						1							
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	SPT	N-Valu	ies	SP1	N-Values	Pror	ortions				SYMBOL	KEY	

- 4							
ı	SPT N-Values	SPT N-Values	Proportions	SYMBOL KEY			
ſ	0 to 4 - Very Loose	0 to 2 - Very Soft	Trace = 0 to 10%	S denotes split-barrel sampler.	7. WH denotes weight of hammer		
1	5 to 10 - Loose	3 to 4 - Soft	Little = 10 to 20%	ST denotes 3-inch O.D. undisturbed sample.	8. WR denotes weight of rods		
1	11 to 30 - Medium Dense	5 to 8 - Medium Stiff	Some = 20 to 35%	3. UO denotes 3-inch Osterberg undisturbed sample.	PP denotes Pocket Penetrometer.		
1	31 to 50 - Dense	9 to 15 - Stiff	And = 35 to 50%	4. PEN denotes penetration length of sampler.	10. FVST denotes field vane shear test.		
-	Over 50 - Very Dense	16 to 30 - Very Stiff		5. REC denotes recovered length of sample.	11. RQD denotes Rock Quality Designation.		
- 1		Over 30 - Hard		SPT denotes Standard Penetration Test.	12. C denotes core run number.		

<sup>2)</sup> Water level readings have been made at times and under conditions stated, fluctuations may occur due to other factors.



## PROPOSED HABITAT FOR HUMANITY DEVELOPMENT

COLBY DRIVE

LEDYARD, CONNECTICUT

 BORING NO.
 B-6

 SHEET
 1 of 1

 FILE NO.
 0015-046.00

 CHKD. BY
 TJO

Boring Co.	General Borings, Inc.	Boring Location	See Boring Location Plan						
Oriller	Jim Casson	Ground Surface El.	308'+/-	Datum	Not Available				
ogged By	Mateusz Fekieta	Date Start	11/5/2024	Date End	11/5/2024				

Hammer Type:	Automatic Hammer	Groundwater Readings (from ground surface)									
Sampler Size:	1-3/8" I.D. Split Spoon	Date	Time	Depth (ft)	Elev.	Stabilization Time					
Type Drill Rig:	Truck Mounted Diedrich D-50	11/5/24	-	-	-	Not Encountered					
Drilling Method:	3.25-inch I.D. Hollow-Stem Augers										

D E P	Casing		SAI	MPLE INFO	RMATION			SAMPLE DESCRIPTION	STRATA
Т Н	Blows (ft)	Type & No.	REC/PEN (inches)	DEPTH (feet)	BLOWS PER 6 INCHES	Core Time (min./ft)			
1		S-1	10/24	0 to 2	2-4-13-26			Medium dense, dark brown, fine SAND, some Silt	8"+/- Topsoil
2								Medium dense, dark brown, line SAND, some Sill	SUBSOIL
3		S-2	18/24	2 to 4	6-11-16-18		Mediu	m dense, gray, fine to coarse SAND, little fine to coarse Gravel, little Silt	
4									TILL
5		S-3	18/24	4 to 6	17-20-34-50		Very de	ense, light gray, fine to coarse SAND, little fine to coarse Gravel, little Silt	
6								ND OF EXPLORATION AT 6 FEET BELOW GROUND SURFACE	
7 8							i	IND OF EXPLORATION AT 6 FEET BELOW GROUND SURFACE	
9						1			
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ı	SPT N-Values	SPT N-Values	Proportions	SYMBO	L KEY
ſ	0 to 4 - Very Loose	0 to 2 - Very Soft	Trace = 0 to 10%	S denotes split-barrel sampler.	7. WH denotes weight of hammer
1	5 to 10 - Loose	3 to 4 - Soft	Little = 10 to 20%	ST denotes 3-inch O.D. undisturbed sample.	8. WR denotes weight of rods
1	11 to 30 - Medium Dense	5 to 8 - Medium Stiff	Some = 20 to 35%	3. UO denotes 3-inch Osterberg undisturbed sample.	PP denotes Pocket Penetrometer.
1	31 to 50 - Dense	9 to 15 - Stiff	And = 35 to 50%	4. PEN denotes penetration length of sampler.	10. FVST denotes field vane shear test.
-	Over 50 - Very Dense	16 to 30 - Very Stiff		5. REC denotes recovered length of sample.	11. RQD denotes Rock Quality Designation.
- 1		Over 30 - Hard		SPT denotes Standard Penetration Test.	12. C denotes core run number.

- 2) Water level readings have been made at times and under conditions stated, fluctuations may occur due to other factors.
- 3) Cobbles and/or boulders were inferred based on observed auger chatter from about 0 to 5 feet below grade.
- 4) Multiple auger refusals between 2 to 5 feet below grade on inferred boulders.



## PROPOSED HABITAT FOR HUMANITY DEVELOPMENT

COLBY DRIVE

LEDYARD, CONNECTICUT

BORING NO. B-7

SHEET 1 of 1

FILE NO. 0015-046.00

TJO

CHKD. BY

Boring Co.	General Borings, Inc.	Boring Location		See Boring Loca	ation Plan
Driller	Jim Casson	Ground Surface El.	310.5'+/-	Datum	Not Available
Logged By	Mateusz Fekieta	Date Start	11/5/2024	Date End	11/5/2024

Hammer Type:	Automatic Hammer	Groundwater Readings (from ground surface)									
Sampler Size:	1-3/8" I.D. Split Spoon	Date	Time	Depth (ft)	Elev.	Stabilization Time					
Type Drill Rig:	Truck Mounted Diedrich D-50	11/5/24	-	-	-	Not Encountered					
Drilling Method:	3.25-inch I.D. Hollow-Stem Augers										

D	ing Method: 3.25-inch I.D. Hollow-Stem A				3.25-Inch I.D. Hollov	w-Stem Aug	gers		
E P	Casing		SAI	MPLE INFO	RMATION			SAMPLE DESCRIPTION	STRATA
T H	Blows (ft)	Type & No.	REC/PEN (inches)	DEPTH (feet)	BLOWS PER 6 INCHES	Core Time (min./ft)			
1		S-1	14/24	0 to 2	2-4-3-4				9"+/- Topsoil
2								Loose, brown, fine SAND, some Silt, trace (-) Roots	SUBSOIL
3		S-2	16/24	2 to 4	8-12-16-23		Modiur	n dense, gray, fine to coarse SAND, little fine to coarse Gravel, little Silt	
4							ivicului	in dense, gray, fine to coarse SAND, little line to coarse Graver, little Silt	TILL
5		S-3	16/24	4 to 6	20-22-40-56		Verv de	ense, light gray, fine to coarse SAND, little fine to coarse Gravel, little Silt	1122
6									
7							E	ND OF EXPLORATION AT 6 FEET BELOW GROUND SURFACE	
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39 40						$\vdash$			
40	SPT N-Values SPT N-Values Pro			Duon	ortions	SYMBOL KEY			

_					
	SPT N-Values	SPT N-Values	Proportions	SYMBO	L KEY
Г	0 to 4 - Very Loose	0 to 2 - Very Soft	Trace = 0 to 10%	S denotes split-barrel sampler.	7. WH denotes weight of hammer
1	5 to 10 - Loose	3 to 4 - Soft	Little = 10 to 20%	ST denotes 3-inch O.D. undisturbed sample.	8. WR denotes weight of rods
Т	11 to 30 - Medium Dense	5 to 8 - Medium Stiff	Some = 20 to 35%	3. UO denotes 3-inch Osterberg undisturbed sample.	PP denotes Pocket Penetrometer.
Т	31 to 50 - Dense	9 to 15 - Stiff	And = 35 to 50%	4. PEN denotes penetration length of sampler.	10. FVST denotes field vane shear test.
1	Over 50 - Very Dense 16 to 30 - Very Stiff			<ol><li>REC denotes recovered length of sample.</li></ol>	11. RQD denotes Rock Quality Designation.
1		Over 30 - Hard		SPT denotes Standard Penetration Test.	12. C denotes core run number.

<sup>2)</sup> Water level readings have been made at times and under conditions stated, fluctuations may occur due to other factors.

<sup>3)</sup> Cobbles and/or boulders were inferred based on observed auger chatter from about 0 to 4 feet below grade.

# **APPENDIX H**

**Outlet Protection Sizing** 



## **ENGLISH OUTLET PROTECTION**

	Habitat for Humanity - Ledyard CT - 0725-500010.00																											
	RIPRAP APRON												SCOUR HO	LE			-	QUANTI	TIES									
Table 11-12																												
			Design	Design	Vel.	TW	Define	d	Botto	n Side	Riprap	SCOUR	La	La	S	MAX.						Stone						Volume of
System	Pipe Rise	Pipe Span	Year	Q	(ft/s)	depth	Channe	el TV	/ Widtl	Slope	APRON	HOLE?	APRON	Minimum	BED	Shear str.	RIPRAP	APRON	APRON	Type	$\frac{Rp^2}{(Q/Rp^{2.5})^{1.333}}$	Size	Type	F	С	В	Area of Riprap	Riprap
Outlet	(in)	(in)	(yr)	(cfs)		(ft)	(Y/N)	Con	d. (ft)	H:1V	TYPE	(Y/N)	LENGTH	(ft)	SLOPE	(lb/ft²)	TYPE	WIDTH 1	WIDTH 2	1 or 2	TW	(ft)		(ft)	(ft)	(ft)	(ft²)	(CUY)
						(1)		(2			(3)	(4)	(5)	(4)		(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(14)	(14)		
FE - 1-1/1-2	24	24	25	10.76	3.43	0	No '	▼ Mi	3	3:01	Α	No ▼	13.7	12	*	*	Modified	6.00	15.57	N/A ■	*						147.4	5.5
FE - 2	12	12	25	0.00	0	0	No '	Mi	1 *	*	Α	No 🔻	1.0	10	*	*	Modified	3.00	10.00	N/A ■	*						65.0	2.4
FE - 3	15	15	25	0.71	2.75	0	No '	Mi	1 *	*	Α	No 🔻	4.5	10	*	*	Modified	3.75	10.75	N/A ■	*						65.0	2.4
FE - 4/5	36	36	25	21.44	8.61	0	No '	Mi	1 *	*	Α	No 🔻	15.7	14	*	*	Inter.	9.00	19.99	N/A ■	*						224.2	12.5

Color Legend:
User Input Calculated

The following are refernces to the CTDOT Drainage Manual:

(1) For a "free outfall" condition use the normal depth of the pipe as an approximation.
(2) Min = TW<.5(Pipe Rise), Max=TW≥.5(Pipe Rise), \* - Does not apply to a well defined channel</li>
(3) Apron type from Section 11.13.5

(4) Scour Houle?: Table 11-12.1 or Table 11-13.1 (Use column (2) to determine which table to use.)

If the velocity in column "F" is > 14fps Then a Scour Hole is required.

(5) Computed La (11.31 or 11.32)

(6) Max. Shear Stress from equation (7.12)

(7) Riprap: Type C Table 7-4
Type A & B Table 11-11 (8)Width 1: Type A & B = 3(Pipe Rise)

Type C = Comps worksheet (W<sub>3</sub>)

(9) Width 2: Type A = 3(Pipe Rise)+.7(La)

Type B = 3(Pipe Rise)+.4(La)Type C = Width 1

(10) Scour Hole Type: Type 1: Depth = .5(Pipe Rise)

Type 2: Depth = Pipe Rise

(see Figure 11-15)

(11) Common part of equation for stone size (d<sub>50</sub>)

(see equations: 11.35 and 11.36)

(12) Stone size (d<sub>50</sub>)

(see equations: 11.35 and 11.36)

(13) Type of Riprap required based on the stone size in (11)

(see Chart on page 11.13-5)

(14) Scour Hole dimensions (see Figure 11-15)



[Date] 500010.00\_OutletProt-English Page 1

# **APPENDIX I**

Grading & Drainage Plan



